

City of Merced

Storm Drain Master Plan *City Project No. 199036*

Final Report
April 19, 2002



Stantec

Stantec File No. 84010156

**CITY OF MERCED
STORM DRAIN MASTER PLAN**

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EXECUTIVE SUMMARY

This report describes and presents the recommended Storm Drain Master Plan (SDMP) proposed for implementation for the City of Merced, California. The purpose of this SDMP is to provide a reference document that will facilitate the planning and implementation of drainage infrastructure improvements required to accommodate stormwater runoff under buildout conditions per the City of Merced Vision 2015 General Plan. The City's Specific Urban Development Plan area is the overall area of study in this SDMP.

The following standards have been applied to the formulation of required drainage infrastructure recommended herein:

- *Storm Drainage Conveyance Elements (Storm Drains and Open Channels)* – 10-year return period storm.
- *Stormwater Detention Basins* – 50-year return period storm under upstream buildout conditions (Inflow); 2-year return period storm under existing upstream conditions (Outflow).

This SDMP does not address regional flood control issues and proposals dealing with major streams passing through the City of Merced (such as Bear Creek and Black Rascal Creek and tributaries) or storm drainage requirements and issues associated with the future UC Merced campus.

In this SDMP, the overall area of study has been broken down into eleven (11) primary local watersheds, Watersheds A through K. Accordingly, recommended storm drainage infrastructure elements have been categorized (or grouped) for each of these watersheds. These watersheds are depicted on Figure ES-1 within this Executive Summary and on Exhibits A and B of this SDMP. A summary of the total storm drainage infrastructure implementation costs attributable to each watershed is provided in Table ES-1 within this Executive Summary, with more detailed cost data being provided on Table 7 of this SDMP.

FIGURE ES-1

CITY OF MERCED STORM DRAIN MASTER PLAN MAP DEPICTING PRIMARY WATERSHEDS CITY OF MERCED JOB NO. 199036 FINAL

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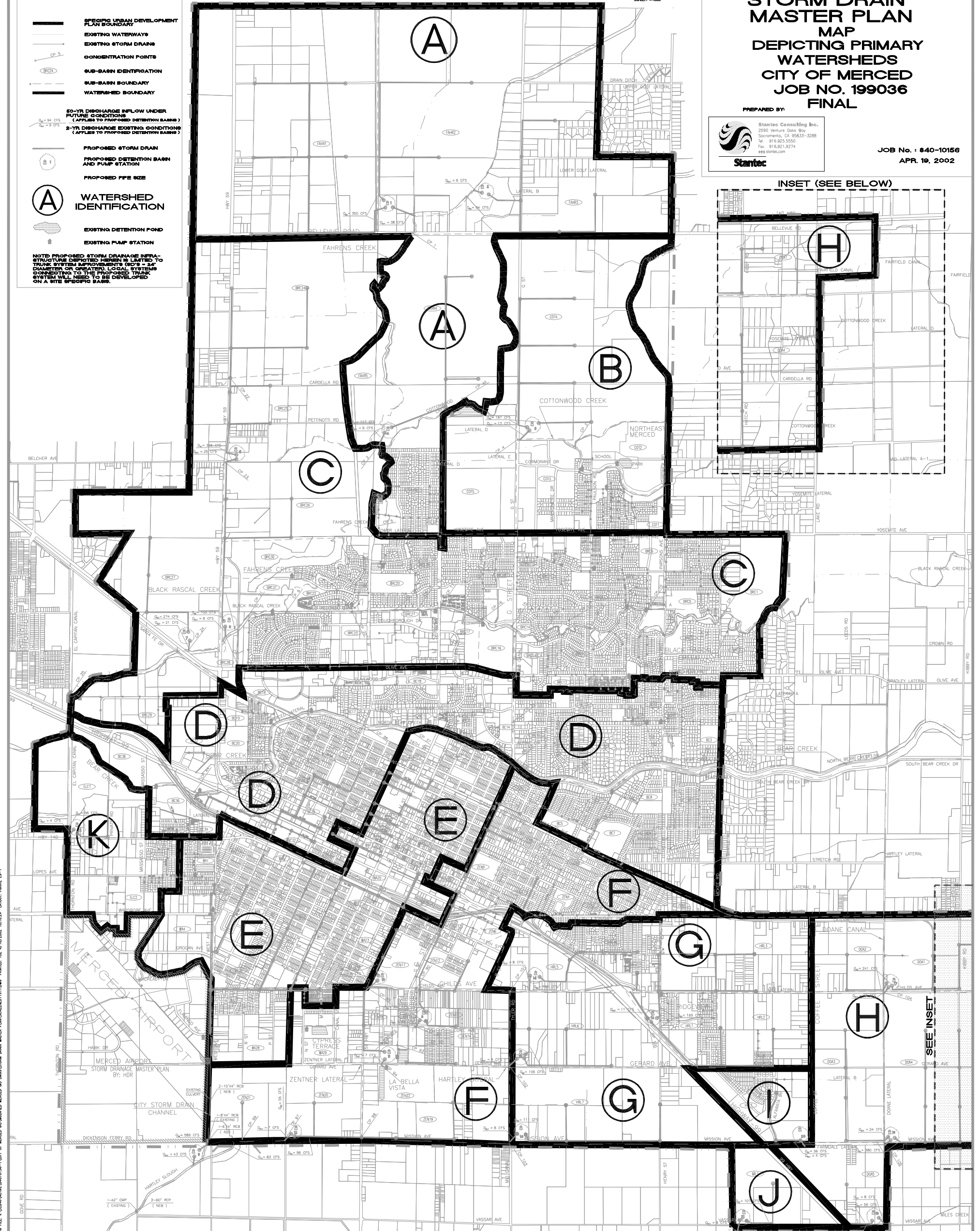
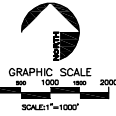


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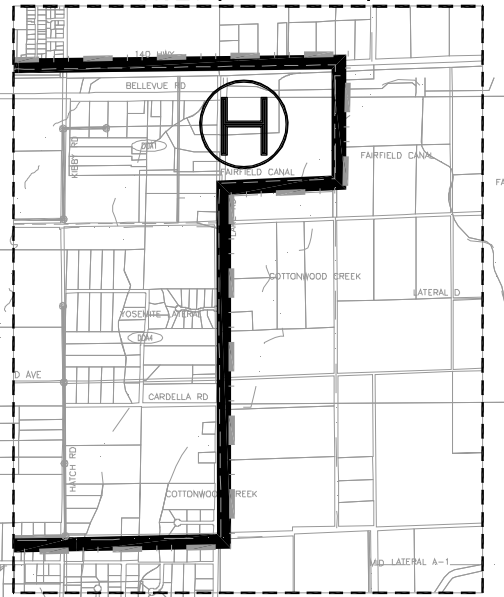
LEGEND

- EXISTING URBAN DEVELOPMENT
- EXISTING WATERWAYS
- EXISTING STORM DRAINS
- CONCENTRATION POINTS
- SUB-BASIN IDENTIFICATION
- SUB-BASIN BOUNDARY
- WATERSHED BOUNDARY
- 50-YR DISCHARGE INFLOW UNDER FUTURE CONDITIONS (APPLIES TO PROPOSED DETENTION BASINS)
- 2-YR DISCHARGE EXISTING CONDITIONS (APPLIES TO PROPOSED DETENTION BASINS)
- PROPOSED STORM DRAIN
- PROPOSED DETENTION BASIN AND PUMP STATION
- PROPOSED PFE SIZE
- WATERSHED IDENTIFICATION
- EXISTING DETENTION POND
- EXISTING PUMP STATION

NOTE: PROPOSED STORM DRAINAGE INFRA-STRUCTURE DEPICTED HEREIN IS LIMITED TO TRUNK SYSTEM IMPROVEMENTS (8" TO 24" DIAMETER OR GREATER). LOCAL SYSTEMS CONNECTING TO THE PROPOSED TRUNK SYSTEM WILL NEED TO BE DEVELOPED ON A SITE SPECIFIC BASIS.



INSET (SEE BELOW)



SEE INSET

TABLE ES-1

**Summary of Estimated Costs
For Storm Drainage Infrastructure**

| Watershed | Outfall | Cost |
|------------------|--|----------------------|
| A | Area Draining into Fahrens Creek | \$ 15,395,142 |
| B | Area Draining into Cottonwood Creek | \$ 4,061,540 |
| C | Area Draining into Black Rascal Creek | \$ 13,754,398 |
| D | Area Draining into Bear Creek | \$ 3,774,722 |
| E | Area Draining into West Avenue Storm Drain | \$ 11,923,408 |
| F | Area Draining into Zentner Lateral Canal | \$ 9,354,450 |
| G | Area Draining into Hartley Lateral Canal | \$ 10,287,256 |
| H | Area Draining into Doane Lateral Canal | \$ 11,657,884 |
| I | Area Draining into Farmdale Lateral | \$ 962,836 |
| J | Area Draining into Miles Creek | \$ 1,357,538 |
| K | Area Draining into El Capitan Canal | \$ 1,129,100 |
| TOTAL | | \$ 83,658,274 |

INTRODUCTION

This report describes and presents a recommended Storm Drain Master Plan (SDMP) for the City of Merced, California. The purpose of this SDMP is to provide a reference document that will facilitate the planning and implementation of drainage infrastructure improvements required to accommodate stormwater runoff under buildout conditions per the City of Merced Vision 2015 General Plan (General Plan). The City's Specific Urban Development Plan (SUDP) area is the overall area of study in this SDMP.

This SDMP has been prepared based on a review of existing information provided by the City of Merced, field reconnaissance, hydrologic analysis, hydraulic analysis, and input and directives from the City Council and City staff. Storm drainage infrastructure has also been formulated in consideration of existing planning documents, studies, and regulations. Cost estimates for implementation of various elements of the storm drainage infrastructure plan are also provided, along with recommendations pertaining to phasing and implementation priorities.

Based on direction provided by the City Council in June 2001, the storm drainage conveyance infrastructure recommended herein has been sized to accommodate runoff generated during a 10-year storm event under upstream buildout conditions per the General Plan. This is a standard that is utilized by many communities in Northern California. Per existing City standards, new stormwater detention basins recommended in this SDMP are sized to accommodate runoff generated during a 50-year storm by the contributing local watershed under buildout conditions per the General Plan, with the peak rate of outflow being limited to the discharge generated by the upstream local watershed during a 2-year storm under existing conditions.

Regional flood control issues and proposals dealing with major streams passing through the City of Merced (such as Bear Creek and Black Rascal Creek and tributaries) are outside of the scope of evaluation covered in this SDMP. This SDMP also does not address storm drainage requirements and issues associated with the future UC Merced campus.

PREVIOUS STUDIES

The following storm drainage master plans that were previously prepared address storm drainage concerns within the City of Merced:

- *1956 Storm Drain Plan (Adamson)*
- *1983 Merced County Critical Area Flooding and Drainage Plan (Nolte and Associates)*
- *2000 City of Merced Airport Storm Drainage Master Plan (HDR)*
- *2001 City of Merced Storm Drain Master Plan, Prototype Watershed Study (Stantec Consulting)*

1956 Storm Drain Plan

This storm drain plan was an early study of watersheds and proposed storm drainage facilities.

1983 Merced County Critical Area Flooding and Drainage Plan

The 1983 study was a master drainage study for a large area of Merced County (approximately 180 square miles located on the east side of the San Joaquin River and south of the Merced River). The 1983 study included the Cities of Livingston, Atwater and Merced as well as other communities.

2000 Airport Storm Drainage Master Plan

The Airport Storm Drainage Master Plan covers the area of the Merced Airport, generally bounded by Wardrobe Avenue on the north, West Avenue on the east, Thornton Road on the west and Dickenson Ferry Road on the south. The study also included two sub-basins within the existing development area northeast of the Airport. This analysis concentrated on identifying existing local flooding conditions and proposed solutions for this limited area. The current SDMP has merely adopted most of the information presented in the Airport Storm Drainage Master Plan.

2001 Prototype Watershed Study

Per City direction, a prototype analysis of the central watersheds within the City of Merced was performed at the early stages of preparing the current SDMP. These two prototype watersheds were named the Central Merced Watershed and the South Area Watershed by the City. The Central Merced Watershed included the existing developed area generally residing between Bear Creek on the north and west, G Street on the east

and the alignment of Highway 99 on the south. The South Area Watershed included the existing development area contiguous to the south of the Central Merced Watershed between roughly the alignment of Highway 99 on the north, West Avenue on the west, Childs Avenue on the south and G Street on the east. The prototype analysis included the following:

- *A hydrologic analysis using the HEC-1 computer model assuming upstream buildout conditions to estimate 10, 50 and 100-year peak discharges at several key locations.*
- *Determination of existing storm drain trunk line capacities and formulation of drainage “trunk” infrastructure required to bring the prototype watershed up to the existing City Standard (10-year storm).*
- *Estimated costs for implementation of the recommended storm drainage capital improvements.*
- *Rough approximation of the cost to upgrade the proposed system to a 100-year storm design level.*
- *Estimation of the cost per residential unit and commercial/industrial acre to fund the proposed improvements required to achieve City Standard (10-year) and to achieve a 100-year design level.*
- *Presentation to the City Council.*

The results of the prototype watershed analysis were presented to the City Council on June 4, 2001 along with a request for City Council direction regarding the “storm return period level of service (10-year or 100-year)” to apply to the preparation of the overall SDMP. The City Council directed the City Engineer to use the 10-year storm return period (existing City Standard) as the standard to size the proposed storm drain system for the overall SUDP area. In providing their direction, the City Council considered information presented to them pertaining to existing system capacities within the prototype watersheds, magnitude of prior storm events that produced documented flooding in the area, standards applied by other Northern California communities, and project implementation costs.

EXISTING DRAINAGE FACILITIES

The City of Merced has constructed a number of drainage facilities within the SUDP area to serve urban development and to provide a drainage network that ultimately drains to a suitable outfall. Existing drainage facilities in the study area generally consist of underground storm drain systems, detention ponds, underground storage pipes, pump stations and open channels.

The City has three major storm drain outfall systems that serve the area south of Bear Creek; the West Avenue storm drain trunk line which flows into Hartley Slough, the Auto Center Drive storm drain system that discharges into Bear Creek and the G Street storm drain which flows southward from Bear Creek into the Zentner Lateral (MID Canal) near Cone Avenue. There are numerous smaller storm drain systems serving smaller developed areas within local sub-basins that drain into Bear Creek, Black Rascal Creek, Fahrens Creek, Parkinson Creek and Cottonwood Creek.

Most of the existing storm drain systems do not have the capacity to convey the 10-year discharges that contribute to them. The storm drain systems within the downtown area (south of Bear Creek) have an average capacity roughly between the 2-year and 5-year storms and the remaining existing storm drain systems have an average capacity generally ranging between the 5-year and 10-year storms.

The City of Merced also operates and maintains several detention ponds, underground storage pipes and pump stations.

Exhibit A shows the location of existing storm drainage facilities, and Tables 5 and 6 show the capacities of existing stormwater storage facilities (detention/retention basins) and pump stations, respectively.

HYDROLOGY

Watershed Descriptions

The SDMP covers the City's Specific Urban Development Plan (SUDP) area that is generally bounded by Nevada Road on the north; Hillcrest Road, Golf Road, Gardner Avenue, McKee Road and California Drive on the east; Vassar Avenue and Mission Avenue on the south; and Thornton Road and Branam Road (west of Highway 59) on the west. The study area is approximately 31 square miles in area and includes a combination of residential, commercial, industrial, institutional, and recreational development and undeveloped agricultural land. Under existing conditions, approximately 50 percent of the study area remains undeveloped. Based on the General Plan, the remaining undeveloped areas are primarily planned for future residential and commercial/industrial uses. This SDMP has been prepared under the assumption that buildout conditions exist for the overall SUDP area.

Based on initial watershed delineations and categorizing areas having a common existing or proposed drainage outfall, the study area has been subdivided into eleven (11) primary local watersheds, Watersheds A through K. Each watershed has been further subdivided into sub-basins. In the hydrologic analysis, there are a total of 142 sub-basins ranging in size from nine (9) acres to 1,184 acres. Exhibit A depicts watersheds and sub-basin boundaries. The following is a brief description of each watershed under existing conditions:

Watershed A

Watershed A is located in the north portion of the study area and contributes runoff into Fahrens Creek. This watershed is approximately 6.3 square miles in area and mainly consists of agricultural land, with a limited number of residential structures associated with agricultural activities. No major storm drain system exists in this watershed except in the small residential area west of M Street and north of Yosemite Avenue.

Watershed B

Watershed B is approximately 2 square miles in area and drains into Cottonwood Creek. This watershed is bounded by Bellevue Road on the north, Sells Lateral Canal on the east, Yosemite Avenue on the south and G Street on the west. Watershed B also consists primarily of agricultural land uses, with some single family residential subdivisions south of Cottonwood Creek. Only the residential area is served by existing storm drainage systems, which include storm drains, underground storage detention pipes and pump stations.

Watershed C

Watershed C is a large watershed that drains into Black Rascal Creek at several locations. The total area of this watershed is approximately 7 square miles. The eastern portion of the watershed (about one-half) is currently developed and consists primarily of residential and commercial land uses. The western and northwestern portion consists of mostly agricultural land use. There is a network of storm drain systems serving the existing residential areas. The existing storm drainage systems include storm drain pipes, underground and surface detention facilities and pump stations.

Watershed D

Watershed D includes the areas that drain into Bear Creek from McKee Road on the east to Highway 99 on the west. This watershed is approximately 3.6 square miles and consists of a mix of residential, commercial and industrial land uses. A network of storm drain systems exist in this watershed and discharge into Bear Creek at various locations. The southwest portion of this watershed is located within the downtown area west of O Street and north of Highway 99. Within the downtown portion of this watershed, a larger storm drain system originates near 22nd Street and S Street and delivers flow to an existing detention basin at the west end of Auto Center Drive where it is discharged into Bear Creek via a pump station.

Watershed E

Watershed E is approximately 2.4 square miles and ultimately drains into the West Avenue storm drain system near the Merced Airport. The watershed is primarily developed with residential land uses, with a degree of commercial and industrial land uses near and north of Highway 99. Runoff from this watershed originates south of Bear Creek near 27th Street and Canal Street and flows into a storm drain trunk line that extends south along O Street to Childs Avenue, then west along Childs Avenue to West Avenue. The West Avenue storm drain system serves as an outfall for nearly one half of the City's existing storm drainage system. At the south end of West Avenue, south of Flamingo Avenue, an 84 inch storm drain discharges to an open channel (lower channel) owned and operated by the City of Merced. The channel continues south into the Merced Airport and passes beneath the approach to the runway via two 84 inch inverted siphon pipelines that drain into another open channel that eventually discharges into Hartley Slough to the south. The West Avenue storm drainage system also carries the Merced Irrigation District (MID) flows during the irrigation season (April 31 to October 31). A pump station at Riggs Avenue lifts irrigation water into the adjacent MID Canal (upper channel) during this period. During the non-irrigation season, stormwater in the storm drain system flows into the lower channel owned and operated by the City of Merced.

Watershed F

Watershed F drains into the Zentner Lateral (MID Canal). The upper portion of the watershed is bounded by Santa Fe Avenue on the north and east, G Street on the west and Yosemite Parkway on the south. The lower portion of the watershed is bounded by Highway 99 on the north, West Avenue on the west, Tyler Road on the east and Mission Avenue/Dickenson Ferry Road on the south. The area of this watershed is approximately 3 square miles. The upper watershed consists primarily of residential land uses and commercial land uses. The existing storm drain system within this area drains to the G Street storm drain which discharges into the Zentner Lateral near Cone Avenue south of Childs Avenue. The lower portion of the watershed is approximately 80 percent agricultural land use and 20 residential land use. There is no major storm drain system currently serving the lower portion of this watershed. Runoff generated in this area flows directly into the Zentner Lateral which discharges into Hartley Slough near the intersection of Dickenson Ferry Road and the south extension of West Avenue.

Watershed G

Watershed G is located in the southeast portion of the study area. This watershed is approximately 3 square miles in area and is bounded by Yosemite Parkway (Highway 140) on the north, Tyler Road on the west, Coffee Street on the east and Mission Avenue on the south. Runoff from this watershed drains into the Hartley Lateral (MID Canal) which discharges into Miles Creek near Tyler Road and Vassar Avenue. Highway 99 bisects this watershed from northwest to southeast. The northeast portion is mainly residential and commercial with some agricultural land use. The area south and west of Highway 99 is mostly agricultural land. There is a pump station near Parsons Street and Childs Avenue which pumps flow from a storm drain system within an existing subdivision into the Hartley Lateral. The remainder of the watershed does not contain any major storm drain systems. Runoff from this area flows into the Hartley Lateral by surface flow.

Watershed H

Watershed H is located in the extreme southeast corner of the study area. The land use in this watershed is mainly consists of agricultural land with some scattered residential units (farm houses). Runoff generated within this watershed flows into the Doane Lateral (MID Canal) which discharges into Miles Creek south Vassar Avenue and Highway 99. The total area of this watershed is approximately 2.7 square miles. There is no storm drain system serving this watershed.

Watershed I

Watershed I is approximately 166 acres in area (0.26 square miles) and is bordered by Gerard Avenue on the north, Coffee Street on the east, Mission Avenue on the south and Highway 99 on the west. Runoff from this watershed flows into the Farmdale Lateral

(MID Canal) near Mission Avenue and Alfarata Boulevard. Approximately 40 percent of this watershed is developed and consists of residential and commercial land use.

Watershed J

Watershed J is located west of Highway 99 between Mission Avenue and Vassar Avenue. It covers an area of approximately 170 acres (0.27 square mile). Runoff from this watershed flows into Miles Creek south of Vassar Avenue. Land use within this area is approximately 70 percent agricultural and 30 percent industrial. This watershed does not have any significant existing storm drain facilities.

Watershed K

Watershed K is located in the southwest portion of the study area just north of the Merced Airport. The watershed area is approximately 500 acres in area (0.78 square miles) and drains into the El Capitan Canal along Thornton Road. Land use within this watershed consists of residential, agricultural and industrial. The east and west portions of the watershed are served by an existing storm drain system that drains into a small local detention basin. The detention basin is equipped with a pump station that discharges flow into the El Capitan Canal. The rest of the area drains by surface flow into the canal.

Watershed Modeling

The U.S. Army Corps of Engineers' (COE) HEC-1 computer program was used to develop a rainfall/runoff computer simulation for the study area. The computer model develops a runoff hydrograph for individual sub-basins through the input of numerical representations of their physical and hydrological characteristics. The computed hydrographs are then routed and/or combined with hydrographs from other sub-basins to yield a dynamic numerical analysis of peak discharges that may be expected to occur at a number of key concentration points along a given flow path. The HEC-1 model was used to estimate flow discharges that would be expected at key locations within the study area during the 10-, 50- and 100-year storm events.

The input parameters utilized for sub-basins in the HEC-1 analysis are presented on Table 1 and are described in the following paragraphs:

Sub-basin Delineation

The boundaries for each sub-basin were determined based on field investigations, U.S. Geological Survey 7.5 minute quadrangle maps, a current aerial photograph at approximate scale of 1"=1000' covering the SUDP, maps contained in the 1956 Storm Drain Plan (revised Jan. 12, 1960), City of Merced Sewer and Storm Drain Plans, and the 1983 Merced County Critical Area Flooding and Drainage Plan. The location of existing

roadways, irrigation canals, storm drains, drainage channels and railroads were incorporated into the establishment of some sub-basins boundaries.

Watershed Soil Type

Watershed soil groups were determined using soil maps contained in a report entitled “Soil Survey of Merced Area, California”, revised March 1991, prepared by the Natural Resources Conservation Service (NRCS).

Rainfall Loss

Rainfall loss is that portion of the precipitation depth that is lost due to evaporation, interception by vegetation, infiltration into soil, and surface depression storage. Rainfall excess is that portion of the precipitation depth that appears as surface or collected storm runoff during and after a storm event. Rainfall losses in this study were determined using the NRCS Curve Number (CN) Method that uses a soil cover complex for estimating watershed losses. The CN is related to the underlying hydrologic soil group (A, B, C, or D), land use, cover density, and antecedent soil moisture conditions. The four hydrologic soil groups are classified as follows:

- Group A:* *Low runoff potential* soils having high infiltration rates even when thoroughly wetted and consisting chiefly of deep, well-drained sands or gravels. These soils have a high rate of water transmission.

- Group B:* Soils having *moderate infiltration* rates when thoroughly wetted and consisting chiefly of moderately deep to deep, moderately well to well-drained sandy-loam with moderately fine to moderately coarse textures. These soils have a moderate rate of water transmission.

- Group C:* Soils having a *low infiltration* rate when thoroughly wetted and consisting chiefly of silt-loam soils with a layer that impedes downward movement of water, or soils with moderately fine to fine texture. These soils have a slow rate of water transmission.

- Group D:* *High runoff potential* soils having very slow infiltration rates when thoroughly wetted and consisting chiefly of clay soils with a high swelling potential, soils with a permanent high water table, soils with a claypan or clay layer at or near the surface, and shallow soils over nearly impervious material. These soils have slow rate of water transmission.

Land Use

Land uses and percent impervious cover values used in this study are based on Table A-2 of City of Merced Design Standards. The percent impervious area for each sub-basin was estimated by direct measurements of land use from the General Plan and represents an important input parameter in the HEC-1 computer model. The computer model relates the amount of impervious area to the total area of a given sub-basin to estimate the amount of runoff losses attributed to pervious areas.

Rainfall

The 24-hour rainfall depth of 2.06 inches for the 10-year storm and 2.74 inches for 50-year storm events utilized in the hydrologic model were taken from the City Design Standards which are based on California Department of Water Resources (DWR) statistics for the Merced area rain gage data from 1940 to 1974. The 100-year, 24-hour rainfall depth of 2.88 inches as contained in the “*City of Merced Airport, Storm Drainage Master Plan*” was used in this analysis. The rainfall data in said report is based on rain gage data from 1940 to 1998 for the same station.

Unit Hydrograph

For runoff computations from each sub-basin, the NRCS Dimensionless Unit Hydrograph option was utilized in the HEC-1 computer model.

Lag Time

Input data for NRCS dimensionless Unit Hydrograph includes the parameter, TLAG, which is equal to the lag (in hours) between the center of mass of rainfall excess and the peak of the unit hydrograph. Lag time was estimated utilizing the NRCS method of computing the watershed lag value from the time of concentration. The equation is as follows:

$$\text{TLAG} = 0.6 t_c$$

t_c = time of concentration

The time required for storm water to flow in the form of runoff from the most hydraulically remote point in the drainage area to a collection point is called the time of concentration. Time of concentration is the sum of the minimum overland travel time (initial time of concentration) and the gutter flow time. The minimum overland travel time was taken from Table A-2 (City Design Standards) based on land use, and the gutter flow time was calculated by dividing the maximum length of travel in the gutter by the velocity of gutter flow. Due to extremely flat slopes in the study area, a one (1) foot per second average velocity was used for gutter flow.

Routing

Routing of runoff between sub-basins was performed utilizing the Muskingum–Cunge method for open channel flow and the Kinematic Wave method for routing flow through storm drains. The Modified Puls Reservoir Routing method was used to route flow through detention basins.

Results

The results of the HEC-1 analysis are summarized on Table 2, which contains the 10-year peak discharges calculated for individual sub-basins within the study area. The results of this study were compared with the 10-year discharges computed by the Merced Airport Storm Drainage Master Plan and the Merced County Critical Area Flooding and Drainage Plan. The peak discharges were compared in terms of cubic feet per second (cfs) per acre. The discharges estimated by HEC-1 for this study are reasonable and compare favorably with the discharges computed by the other two studies. HEC-1 input/output for the 10-, 50-, and 100-year storm events is included in the Appendix.

STORM DRAINAGE INFRASTRUCTURE PLAN

The storm drainage infrastructure plan presented in this SDMP has been formulated to serve the City of Merced Specific Urban Development Plan (SUDP) area. The proposed facilities consist of an integrated system of pipe and channel conveyance systems and detention facilities designed to attenuate (or reduce) peak flow rates generated from the SUDP area. This SDMP only addresses the requirements for the major trunk line (backbone) infrastructure system necessary to provide storm drainage conveyance and control and does not address individual local systems associated with individual developments. All storm drainage “conveyance” facilities specifically presented herein have been sized to accommodate a 10-year storm event. Proposed detention basins are sized for 50-year storm inflow (developed) with an outflow limited to a peak rate equivalent to a 2-year storm discharge that would occur under existing conditions. These parameters conform with existing City Design Standards. Storm drainage infrastructure elements incorporated into the SDMP are depicted on Exhibit B and include the following:

- *Excavated Open Channels*
- *Storm Drains*
- *Stormwater Detention Facilities*
- *Pump Stations*

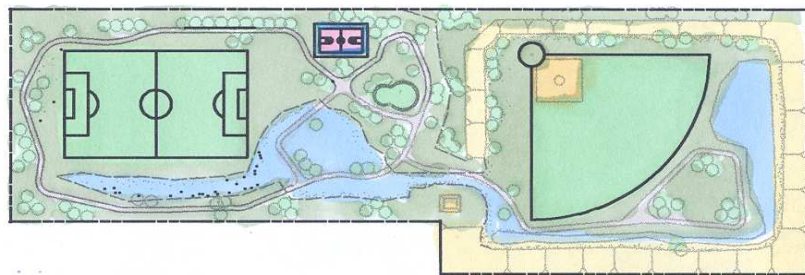
The following is a brief description of the drainage infrastructure components proposed to accommodate stormwater runoff anticipated to occur under General Plan buildout conditions. Assumptions associated with these elements have been incorporated into the HEC-1 hydrologic model for the master plan condition provided in the Appendix..

Excavated Open Channels – 60-foot right-of-way (R/W) channels are proposed to convey runoff through areas where the estimated peak flow rates from a watershed exceed the capacity of a 66” storm drain in areas that are not currently developed. Open channels are proposed in Watershed A and Watershed H in the northwest and southeast portions of the study area, respectively. Open channels of lesser width can also be utilized as an option instead of large diameter pipes in areas where adequate ground cover does not exist for large size pipes. In conformance with General Plan policies, these open channels should include landscaping and bike paths to provide linear recreation opportunities. A minimum of one (1) foot of freeboard shall be maintained above the design 10-year water surface elevation to the top of banks. One side of the channel shall provide for all weather maintenance access unless the channel is adjacent to a public road. Exhibit C shows a typical cross-section of a typical open channel.

Storm Drains – Underground storm drain pipelines are proposed to be utilized to serve the majority of new development areas and as upgrades to many existing conveyance facilities in existing development areas. The proposed storm drain pipeline conveyance system depicted on Exhibit B consists of the major trunk line (backbone) system and is intended to provide master plan level guidance for future storm drain pipeline design. In areas where cover problems exist, multi-sized smaller diameter pipes or equivalent capacity alternatives can be used in place of the pipe sizes represented in this SDMP. In several locations in the downtown area (south of Bear Creek), where the existing storm drain pipes do not have the capacity to convey the design flows, the option of adding additional storm drains to work in conjunction with existing storm drains is proposed. Storm drain trunk lines are sized to convey the 10-year discharges operating under uniform flow conditions. All proposed storm drain lines are to be located in public streets in the existing developed areas. Exhibit B shows the location and sizes of the proposed storm drain trunk lines.

Stormwater Detention Facilities – Large excavated sites (detention basins) are proposed to be used for the purpose of storing runoff in a manner that significantly reduces peak flows that would otherwise overtax to the available downstream outfall system. Due to capacity limitations associated with the downstream outfall systems, there are 22 detention basins proposed in this SDMP. All of the detention basins are considered to have non-interruptible outlet facilities and have been sized for inflow from a 50-year 24-hour storm (developed condition) with outflow limited to a peak rate generated by a 2-year storm occurring under the existing level of development within the contributing watershed. Due to the close proximity of groundwater to the surface, detention basins have been conceptually designed with a maximum depth of five (5) feet below the existing ground surface, including one (1) foot of freeboard from the 50-year water surface elevation to the top of the basin. This constraint caused the proposed detention basins to have relatively large surface areas and shallow depths. At the time of actual design of the detention basins, the depth and surface area of the detention basins may be adjusted if the actual local groundwater depth is greater than seven (7) feet. Spillways should be provided above the 50-year water surface elevation to control overflow and provide for emergency releases. All proposed detention basins should have vehicular access to the lower areas to facilitate maintenance.

As a part of the actual design of stormwater detention basins recommended in this SDMP, consideration shall be given to the physical and

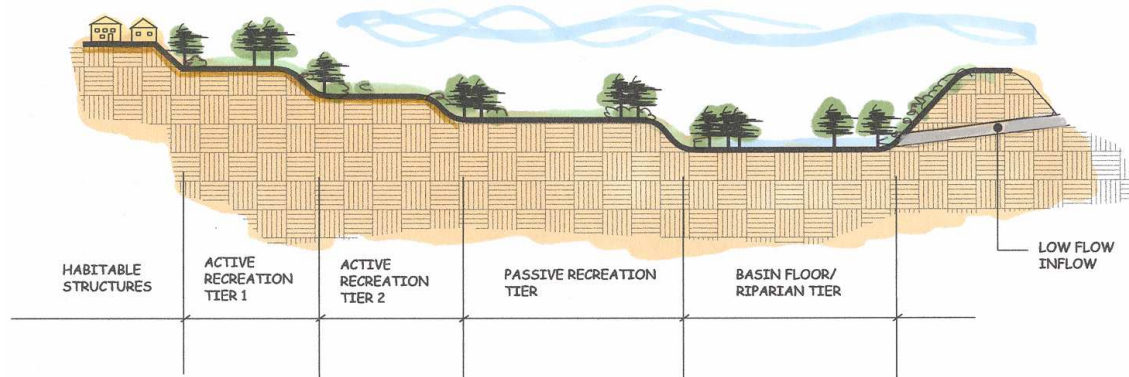


Schematic Joint-Use Detention Basin

and economic feasibility of creating joint-use opportunities for active and passive recreation within these facilities. Active and passive recreation elements, where feasible, shall be appropriately sited in consideration of flood risk and shall be elevated above low flow

areas, ponding areas and other frequently inundated areas. If site conditions, recreation needs and funding create a favorable opportunity for the inclusion of active or passive recreation elements as a joint use within a given stormwater detention facility, the following fundamental design approaches should be utilized:

1. Low flow must be accommodated in a manner that confines the frequent inundation zones to areas that will characteristically require only limited maintenance.
2. Contouring within detention facilities is recommended to create internal elevation variations (or tiers) that have differing frequencies and depths of inundation and flood risk. The following use hierarchy may be utilized as a starting point in evaluating design opportunities:
 - ◆ Lowest lying areas - semi-natural riparian areas, ponds, cleared zones.
 - ◆ Lower elevated tiers - picnic areas, passive turf, and vegetation zones.
 - ◆ Intermediate elevated tiers - ball fields, soccer fields.
 - ◆ Upper elevated tiers - court games, parking areas.
 - ◆ Areas elevated above 100-year flood level - restrooms, habitable structures.



Schematic Cross Section Depicting Tiers Within a Joint-Use Detention Basin

3. Internal drainage within detention facilities should provide for positive flow across elevated tiers and to the basin's lowest lying areas to prevent the nuisance of residual standing water within active and passive recreation areas.
4. Hydraulic design components should be included as needed: inlet and outlet structures, spillways, sediment basins, etc.
5. Basin slopes should be flat enough to allow for mowing of turf areas and other routine recreation-related maintenance activities.

Exhibit B shows the locations and Table 3 contains summary data for proposed detention basins.

Pump Stations – Pumps are used to assist in the draining of stormwater detention basins in locations where gravity controlled structures are not feasible as the sole outflow mechanism. Given the flatness of topography in the study area, detention basins in this SDMP are assumed to be drained by pump stations to a downstream conveyance system. The pump stations have been conceptually sized to pump the 2-year discharges generated under existing land use assumptions. Detention basin pumping facilities are assumed to consist of a low flow pump, a high flow pump and a backup (redundant) pump. Table 4 shows the input data for the proposed pump stations.

EXISTING OUTFALL FACILITIES

The existing outfall facilities (outfall conveyance systems) within the study area consist of natural channels and various Merced Irrigation District (MID) Canals and Laterals. Runoff from existing developed and undeveloped areas within the City's SUDP area currently enters these natural channels and MID Canals. Given that there are currently limitations in downstream system capacities, it is recommended that the peak rates of runoff currently expected should be retained after the proposed storm drain system is in place. This peak rate of runoff is assumed to be the 2-year discharge occurring based on existing levels of development. Under this SDMP, the discharge from proposed developed areas to these outfall facilities has been limited to the 2-year existing condition peak rate of runoff, which will prevent flow in the downstream conveyance system from increasing significantly.

The following natural streams and MID Canals are within or adjacent to the study area and are currently being used as outfall facilities for stormwater runoff generated within the SUDP area:

- *Fahrens Creek*
- *Cottonwood Creek*
- *Black Rascal Creek*
- *Bear Creek*
- *Hartley Slough*
- *MID El Capitan Canal*
- *MID Zentner Lateral*
- *MID Hartley Lateral*
- *MID Doane Lateral*
- *MID Farmdale Lateral*

Fahrens Creek, Cottonwood Creek, Black Rascal Creek and Bear Creek are natural streams and serve as stormwater outfalls for City runoff in addition to their natural function as a drainage channels for flows generated within the hillsides and agricultural areas to the north and northeast of Merced. Fahrens Creek, Cottonwood Creek and Black Rascal Creek are tributaries of Bear Creek and pass through the north side of the SUDP area. Approximately 75 percent (75%) of the study area drains into these streams. Hartley Slough collects City runoff that discharges into it at a location south of the intersection of West Avenue and Dickenson Ferry Road and serves as a stormwater outfall for areas south of the downtown area as well as a discharge point for some MID Canals and Laterals. The flow carrying capacity of these natural streams range approximately between a 2-year and a 10-year storm event (Ref.1).

The MID Canals and Laterals that collect City runoff are located within the south and southeast portions of the study area generally south of Highway 140 and Childs Avenue. The primary function of these canals and laterals is to deliver irrigation water from Lake Yosemite to downstream agricultural users. They generally convey irrigation water from

the end of April to the end of October. The canals and laterals are also used as stormwater outfalls for City runoff as they traverse the entire study area. Most of the stormwater runoff from area east of G Street and south of Santa Fe Avenue and Highway 140 currently drains into MID Canals and Laterals. The flow carrying capacity of these canals ranges from approximately 20 to 80 cfs (Ref.1).

COST ESTIMATES

Construction cost estimates for primary drainage systems have been prepared for each of the eleven (11) watersheds represented in this SDMP. Table 7, Sheets 1 through 11 are cost estimates for storm drainage infrastructure recommended for each watershed. The recommended drainage systems consist of major storm drain trunk line and open channel conveyance facilities and detention basins to limit flow discharges into the downstream conveyance systems (outfalls). No improvements to the downstream conveyance systems are recommended except for the City's existing storm drain channel in Watershed E (West Avenue) and the upgrade of an existing pump station in Watershed D (Auto Center Drive detention basin).

The cost estimates contained in Table 7, Sheets 1 through 11 are based on estimated quantities and assumed unit costs for construction elements and land acquisition. These unit costs are generalized estimates and are considered to be reasonable for planning purposes. Generalized cost estimating data for pump stations of varying capacities is shown in Table 4. A contingency factor of 15% is added to the basic costs as well as an additional 25% factor to account for design and planning, construction management and program implementation.

PHASING AND PRIORITIES

Based upon economics and funding availability, it would be difficult to financially sustain the construction of the proposed storm drainage facilities all at one time. An appropriate approach is to prioritize improvements and proceed with construction of selected storm drainage improvements as funding becomes available and/or as new development occurs. Priority should be given to improving storm drainage systems in areas that have historically experienced flooding difficulties and on improving or providing storm drainage outfall systems. The next priority would be to provide storm drain improvements within the downtown area (Watersheds D & E) and along G Street and its downstream elements. Since most of the storm drainage facilities proposed in this SDMP are located in the areas which are not currently developed, the third priority will depend upon the location and magnitude of growth and future development within the SUDP area. When development is proposed to occur in any watershed shown on Exhibit B, the storm drainage facilities in the development should be designed to meet the proposed storm drainage system requirements represented in this SDMP.

Under the first phase of priorities, there are eight (8) areas that should be considered for storm drainage upgrades based on information provided by the City regarding existing flooding conditions or potential future flooding. The eight (8) areas have been identified as follows:

- 1- *West Avenue Outfall*
- 2- *Martin Luther King Way/Childs Avenue*
- 3- *McSwain Road (Highway 140)/ Sydney Drive*
- 4- *Stonybrook Avenue*
- 5- *Carol Avenue/Childs Avenue*
- 6- *M Street/21st Street*
- 7- *Paseo Verde Drive/Black Rascal Creek*
- 8- *Auto Center Drive/Bear Creek*

West Avenue Outfall: This phase of the storm drainage improvements is focused around the south end of West Avenue where a single 84” storm drain pipe discharges into the City’s storm drain channel. The City’s storm drain channel commences at Flamingo Avenue (Riggs Road) near the south end of West Avenue and continues south and ultimately discharges into Hartley Slough south of Dickenson Ferry Road. The channel and accompanying downstream facilities between Flamingo Avenue and Hartley Slough are severally undersized to carry the 10-year discharge (400 cfs) generated within Watershed E. The channel transitions to two 84 inch inverted siphons under the approach to the airport runway, then becomes a channel again that drains to a single 8’x 4’ box culvert at Dickenson Ferry Road before discharging into Hartley Slough. The existing channel capacity is approximately between 200 and 300 cfs depending on location. Vegetation growth in the existing channel should be periodically mitigated as historical flows have on occasion escaped the channel banks. Due to capacity limitations in the downstream system, the upstream storm drain system can back up and cause overflow

along the areas of West Avenue and Childs Avenue. These conditions can be alleviated by the implementation of the following improvements:

- *Widening the City's storm drain channel to improve capacity.*
- *Replacing the 84" siphons under the airport runway with two 8'x 4' box culverts.*
- *Adding a 6'x 4' cell to the existing box culvert at Dickenson Ferry Road.*
- *Constructing a stormwater detention basin (Detention Basin 8) with a pump station at the southwest corner of Dickenson Ferry Road and West Avenue.*
- *Replacing the 1-42" corrugated metal pipe (CMP) at the Hartley Slough crossing of Hartley Road and the west extension of Vassar Avenue with two 60" RCPs.*

These proposed improvements will enhance the capacity of the West Avenue storm drain system by lowering the hydraulic grade line in the upstream storm drain pipes.

Martin Luther King Way/Childs Avenue: The City staff has indicated that the intersection of Martin Luther King Way (MLK Way) and Childs Avenue requires storm drainage capacity upgrades. The drainage sub-basin contributing runoff to this intersection is 97 acres and bounded by 13th Street on the north, MLK Way on the west, G Street on the east and Childs Avenue on the south. The area generates approximately 35 cfs during the 10-year storm event. There is no storm drain system along MLK Way except several disconnected catch basins, which provide temporary storage for minor flows. Stormwater runoff concentrating at the intersection of MLK Way and Childs Avenue is conveyed by a 24" storm drain pipe (capacity = 7 cfs) under Childs Avenue to a pump station located in the southeast corner of the intersection. The pump station discharges into the MID Canal along the south side of Childs Avenue. Since MLK Way is also a state highway (Highway 59), the pump station is owned and operated by the California Department of Transportation (CalTrans). According to the City's maintenance staff, the pump station has the capacity of approximately 1,500 gallons per minute (gpm), which is roughly equal to 3.3 cfs. The 24" storm drain under Childs Avenue and the pump station have a capacity that is less than the 2-year discharge (18 cfs). Hence, runoff ponds in MLK Way north of the intersection and in Childs Avenue east of the intersection during many smaller storm events.

In order to reduce the frequency of runoff collecting and ponding in this area, it is recommended that a detention basin be constructed at the northeast corner of MLK Way and Childs Avenue. A new 36" storm drain in MLK Way starting at 13th Street and changing to a 42" at 7th Street will deliver flow into the detention basin. A pump station is proposed to discharge approximately 4 cfs from the detention basin into a proposed 24" outlet pipe that will run south along Highway 59 and discharge into Zentner Lateral (MID Canal) along Gerard Avenue. The proposed storm drainage system for this area is shown on Exhibit B.

McSwain Road (Highway 140)/Sydney Drive: This area consists of single family residential development and is located north of Highway 140 and east of Massasso Street. A storm drain system and a pump station that discharges stormwater runoff to the north into Bear Creek serve the existing development. A portion of the storm drain from Demoss Avenue downstream is a 72" pipe that serves as an under ground stormwater storage facility. The storage volume is approximately 2.2 acre-feet (AF) while the 10-year and 50-year runoff volumes are 3 and 5 acre-feet, respectively. The total capacity of the pump station is 3.6 cfs, and the 10-year discharge from the sub-basin is approximately 10 cfs. It is recommended that the pump station be upgraded to increase the capacity to discharge the runoff generated during the 10-year storm event.

Stonybrook Avenue: This area is located along the west bank of Bear Creek, south of Atchison Topeka and Santa Fe Railroad and east of Highway 59. The area consists of single and multi family residential and a mobile home park. Runoff in the area is collected by a storm drain system and pumped into Bear Creek. A detention basin with storage capacity of approximately 2.2 AF is located north of Willowbrook Drive and west of Stonybrook Avenue. The runoff volumes for the 10-year and 50-year storms are 5 and 7 AF, respectively. The capacity of the pump station is approximately 11 cfs while the 10-year peak discharge is 14 cfs. The comparison of the capacity of existing detention basin and the pump station with the volume and peak discharge from the 10-year storm indicates that the existing facilities do not have the capacity to handle the incoming flow generated within the area. Therefore, it is imminent that flooding will occur in this area during any storm exceeding the 5-year event. It is recommended that the capacity of the existing detention basin and pump station be upgraded to at least the 10-year storm event.

Carol Avenue/Childs Avenue: This area receives runoff from a 50 acre sub-basin bordered by Merced Avenue on the north, Parsons Street on the east, Childs Avenue on the south and Highway 99 on the west. The 10-year discharge at this location is estimated to be 16 cfs. There is an 18" storm drain at the intersection of Carol Avenue and Childs Avenue, which discharges into Hartley Lateral. The 18" storm drain has a capacity of about 3.5 cfs when flowing full (with an assumed slope of 0.1%). Under pressure flow conditions the capacity would be slightly more. The SDMP proposes a 30" storm drain in Carol Avenue starting at a location approximately 600 feet south of Merced Avenue and discharging into Hartley Lateral.

M Street/21st Street: The intersection of M Street and 21st Street is located within the downtown area just east of the Courthouse Square. There is a 54" storm drain (2 blocks west of the intersection) that runs along O Street from 23rd Street to Childs Avenue. A 24" storm drain along 23rd Street and an 18" storm drain along 19th Street connect to the 54" storm drain system. At the intersection of M Street and 21st Street there is a 30" storm drain in M Street between 21st Street and 20th Street which is not connected to any downstream system. Runoff intercepted by this 30" storm drain does not have an outlet, and stormwater accumulates in the pipe and rises to an elevation above the drain inlets and causes flooding of the intersection. The SDMP proposes a 30" storm drain along 21st Street starting at MLK Way and continuing west along 21st Street to M Street, then turning south along M Street to 20th Street. At 20th Street the proposed storm drain

increases to a 36” pipe and connects with the 54” storm drain at O Street. This storm drain will intercept the 10-year runoff generated by area west of G Street between 22nd and 20th Streets.

Paseo Verde Drive/Black Rascal Creek: The drainage area contributing runoff to this vicinity is located west of R Street between the confluence of Fahrens Creek and Black Rascal Creek. The contributing area in the SDMP is designated as sub-basin BRC22 and covers approximately 105 acres, consisting of mainly single family residential. A network of existing storm drains that flow from north to south serves the area and discharges via a pump station into Black Rascal Creek downstream of the R Street bridge. The capacity of the existing pump station is approximately 20 cfs, and the estimated 10-year runoff generated by the contributing area is 25 cfs. No stormwater storage facility exists within this sub-basin. Two other short reaches of storm drain are located in R Street. An 18” storm drain originates at the intersection of R Street and Loughborough Drive and runs north along R Street, discharging into Black Rascal Creek. The second reach (24”) starts just south of Buena Vista Drive and runs south along R Street and flows into Black Rascal Creek. These storm drain systems discharge into the reach of Black Rascal Creek which is located just upstream of the confluence with Fahrens Creek. Backwater created by the confluence of these two creeks may cause the storm drain systems to back up causing local flooding. In order to evaluate flooding in this area further, a more detailed site specific analysis may be required to examine the existing storm drain systems and to determine the cause of flooding.

Auto Center Drive/Bear Creek: Auto Center Drive is located in the downstream portion of the large portion of Watershed D south of Bear Creek and receives runoff from western one half portion of the downtown area. The contributing area is approximately 465 acres and is bounded by Bear Creek on the north and west, O Street on the east and Highway 99 on the south. The 10-year runoff generated by this area is estimated to be approximately 157 cfs. There is a storm drain system that starts at 22nd Street and S Street and continues south along T Street turning west along 16th Street and Auto Center Drive and discharging via a pump station into Bear Creek. The existing storm drain sizes range from 20” at the upstream portion to a maximum of 42” at the western end of Auto Center Drive near the outlet. A pump station is used to discharge flow into Bear Creek. A small (approximately one-acre) overflow detention basin is located to the west of the pump station between the south bank of Bear Creek and Highway 99. The capacity of the pump station is approximately 20 cfs, and the 2-year discharge is estimated to be approximately 100 cfs. During a major storm event, the amount of runoff generated by the drainage area greatly exceeds the capacity of the existing detention basin and pump station and causes the stormwater in the storm drain system to back up and flood the streets and surrounding areas. The SDMP proposes to upgrade the storm drain system and the pump station to convey and discharge the 10-year runoff generated by the watershed. Exhibit B shows the proposed storm drain system.

MITIGATION OF STORMWATER QUALITY

Stormwater quality programs have been mandated by Phase I of the U S Environmental Protection Agency (EPA) program as a part of the National Pollutant Discharge Elimination System (NPDES) under the Clean Water Act (CWA) to regulate municipal and industrial discharges to surface waters of the U S. Phase I of the NPDES Program only impacted industrial sites, construction sites and municipal separate stormwater conveyance systems for communities having a population in excess of 100,000 people. However, on December 8, 1999 the EPA issued rules regarding the forthcoming implementation of Phase II of the NPDES regulations. Phase II of the program will include more than 5,000 U.S. local governments previously not regulated by federal stormwater rules, and these governments will be required to submit NPDES-permitted stormwater management plans by March 2003. Stormwater Phase II regulations will require cities, counties, regional authorities and other units of local government with municipal separate storm sewer systems located in urbanized areas to design, finance, and implement a comprehensive stormwater quality management program. Urbanized areas are defined by the U. S. Census Bureau to contain a cumulative population of 50,000 or more and a minimum average population density of 1,000 people per square mile. Per the General Plan, the City's population is in excess of 60,000 people, and thus, Merced would fall under these Phase II regulations.

The Phase II program requires that the stormwater management plan (SWMP) include a set of six minimum control measures. The six minimum measures are:

- Public education and outreach on storm water impacts
- Public participation/involvement in the SWMP
- Illicit discharge detection and elimination
- Construction site stormwater runoff control for sites one acre or larger
- Post-construction stormwater management for new development and redevelopment
- Pollution prevention/good housekeeping for municipal operations

The SWMP must also identify and implement best management practices (BMPs) and measurable goals for each control measure. These BMPs and goals must be evaluated in annual reports submitted to the Regional Water Quality Control Board. The SWMP must be fully implemented by the end of the first permit term, anticipated to be a five year period.

REFERENCES

- 1- Nolte and Associates, “*Draft Merced County Critical Area Flooding and Drainage Plan*”, January 1983.
- 2- HDR Engineering, “*City of Merced Airport Storm Drainage, Drainage Master Plan*”, February 2000.
- 3- City of Merced, “Standard Designs of Common Engineering Structures”.
- 4- City of Merced, “*Vision 2015- General Plan*”, 1997.
- 5- Natural Resources Conservation Service (NRCS), “*Soil Survey Merced Area, California*”, March 1991.
- 6- Federal Emergency Management Agency, “*Flood Insurance Study, Merced County California and Incorporated Areas*”, August 1995.
- 7- Corps Of Engineers, Hydrologic Engineering Center, “*HEC-1 Flood Hydrograph Package*”, Davis, California, September 1990.
- 8- Federal Emergency Management Agency, “*Flood Insurance Study, Merced County, California, Unincorporated Areas*”, Revised March 1991.
- 9- Environmental Protection Agency, “*40 CFR, Parts 9,122,123,and 124, National Pollutant Discharge Elimination Program – Regulations for Revision of the Water Pollution Control Program Addressing Storm Water Discharges*”, December 1999.

Table 1

Hydrologic Parameters Used in HEC-1 Model

CITY OF MERCED
Storm Drain Master Plan
Hydrologic Parameters Used in HEC-1 Computer Model

Table 1

| Watershed | Outfall | Sub-Basin | Drainage Area (Acres) | Drainage Area (Sq. Mile) | Curve Number | Percent Impervious | Lag Time (hr.) |
|------------------|--|------------------|------------------------------|---------------------------------|---------------------|---------------------------|-----------------------|
| A | Fahrens Creek (Watershed A) | FAHR 1 | 1184 | 1.85 | 80 | 51 | 1.73 |
| A | (Sub-basins Draining into Fahrens Creek) | FAHR 2 | 898 | 1.4031 | 76 | 33 | 1.95 |
| A | | FAHR 3 | 712 | 1.1125 | 72 | 37 | 1.78 |
| A | | FAHR 4 | 595 | 0.9297 | 73 | 37 | 1.28 |
| A | | FAHR 5 | 133 | 0.2078 | 80 | 41 | 0.7 |
| A | | FAHR 6 | 207 | 0.3234 | 71 | 35 | 1.03 |
| B | Cottonwood Creek (Watershed B) | COT 1 | 135 | 0.2109 | 75 | 30 | 0.84 |
| B | (Sub-basins Draining into Cottonwood Creek) | COT 2 | 120.64 | 0.1885 | 79 | 31 | 0.74 |
| B | | COT 3 | 151.1 | 0.236 | 66 | 38 | 0.84 |
| B | | COT 4 | 846.6 | 1.3228 | 76 | 39 | 1.7 |
| B | | COT 5 | 266 | 0.4156 | 67 | 15 | 1.08 |
| C | Black Rascal Creek (Watershed C) | BRC 1 | 152 | 0.2375 | 76 | 30 | 0.76 |
| C | (Sub-Basins Draining into Black Rasca Creek) | BRC 2 | 53.1 | 0.083 | 70 | 30 | 0.45 |
| C | | BRC 3 | 94.52 | 0.1477 | 71 | 28 | 1.01 |
| C | | BRC 4 | 93.55 | 0.1462 | 70 | 29 | 0.78 |
| C | | BRC 5 | 57.51 | 0.0899 | 71 | 30 | 0.53 |
| C | | BRC 6 | 59.4 | 0.0928 | 73 | 32 | 0.62 |
| C | | BRC 7 | 59.97 | 0.0937 | 75 | 30 | 0.53 |
| C | | BRC 8 | 58.14 | 0.0908 | 76 | 30 | 0.74 |
| C | | BRC 9 | 96.99 | 0.1515 | 74 | 29 | 0.83 |
| C | | BRC 10 | 81.44 | 0.1273 | 64 | 30 | 0.62 |
| C | | BRC 11 | 90.11 | 0.1408 | 77 | 35 | 0.78 |
| C | | BRC 12 | 20.66 | 0.0323 | 72 | 39 | 0.47 |
| C | | BRC 13 | 51.31 | 0.0802 | 71 | 30 | 0.87 |
| C | | BRC 14 | 31.34 | 0.049 | 70 | 34 | 0.53 |
| C | | BRC 14B | 49.36 | 0.0771 | 70 | 61 | 0.45 |
| C | | BRC 15 | 49.07 | 0.0767 | 79 | 41 | 0.66 |
| C | | BRC 16 | 43.9 | 0.0686 | 72 | 15 | 0.45 |
| C | | BRC 17 | 68.01 | 0.1063 | 68 | 58 | 0.48 |

CITY OF MERCED
Storm Drain Master Plan
Hydrologic Parameters Used in HEC-1 Computer Model

Table 1

| Watershed | Outfall | Sub-Basin | Drainage Area (Acres) | Drainage Area (Sq. Mile) | Curve Number | Percent Impervious | Lag Time (hr.) |
|-----------|---------------------------------------|-----------|-----------------------|--------------------------|--------------|--------------------|----------------|
| C | | BRC 18 | 209.54 | 0.3274 | 77 | 32 | 0.81 |
| C | | BRC 19 | 44 | 0.0688 | 74 | 30 | 0.83 |
| C | | BRC 20 | 85 | 0.1328 | 74 | 31 | 0.49 |
| C | | BRC 21 | 116.79 | 0.1825 | 71 | 77 | 0.51 |
| C | | BRC 22 | 104.91 | 0.1639 | 77 | 31 | 0.59 |
| C | | BRC 23 | 212.75 | 0.3324 | 64 | 50 | 1.76 |
| C | | BRC 24 | 706 | 1.1031 | 80 | 51 | 1.48 |
| C | | BRC 25 | 380 | 0.5938 | 80 | 58 | 1.07 |
| C | | BRC 26 | 376 | 0.5875 | 79 | 50 | 1.23 |
| C | | BRC 27 | 621 | 0.9703 | 79 | 84 | 1.35 |
| C | | BRC 28 | 32.43 | 0.0507 | 63 | 84 | 0.39 |
| C | | BRC 29 | 188.13 | 0.294 | 72 | 85 | 1.02 |
| C | | BRC 30 | 142 | 0.2219 | 80 | 36 | 0.55 |
| C | | BRC 31 | 78 | 0.1219 | 78 | 32 | 0.62 |
| D | Bear Creek (Watershed D) | BC 1 | 92 | 0.1438 | 67 | 30 | 0.67 |
| D | (Sub-Basins Draining into Bear Creek) | BC 2 | 37.02 | 0.0578 | 77 | 31 | 0.45 |
| D | | BC 3 | 87.81 | 0.1372 | 68 | 31 | 0.78 |
| D | | BC 4 | 156 | 0.2438 | 74 | 30 | 0.78 |
| D | | BC 5 | 74.04 | 0.1157 | 70 | 32 | 0.65 |
| D | | BC 6 | 18.37 | 0.0287 | 61 | 30 | 0.43 |
| D | | BC 7 | 48.78 | 0.0762 | 64 | 23 | 0.69 |
| D | | BC 8 | 54.64 | 0.0854 | 62 | 26 | 0.67 |
| D | | BC 9 | 139.18 | 0.2175 | 65 | 32 | 0.83 |
| D | | BC 10 | 83.16 | 0.1299 | 61 | 38 | 0.58 |
| D | | BC 11 | 11.48 | 0.0179 | 80 | 30 | 0.41 |
| D | | BC 12 | 42.47 | 0.0664 | 73 | 31 | 0.53 |
| D | | BC 13 | 97.57 | 0.1525 | 72 | 32 | 0.99 |
| D | | BC 14 | 149.28 | 0.2333 | 63 | 60 | 0.7 |
| D | | BC 15 | 18.5 | 0.0289 | 61 | 30 | 0.48 |

CITY OF MERCED
Storm Drain Master Plan
Hydrologic Parameters Used in HEC-1 Computer Model

Table 1

| Watershed | Outfall | Sub-Basin | Drainage Area (Acres) | Drainage Area (Sq. Mile) | Curve Number | Percent Impervious | Lag Time (hr.) |
|-----------|---|-----------|-----------------------|--------------------------|--------------|--------------------|----------------|
| D | | BC 16 | 37.5 | 0.0586 | 61 | 30 | 0.53 |
| D | | BC 17 | 30.42 | 0.0475 | 61 | 30 | 0.47 |
| D | | BC 18 | 173 | 0.2703 | 62 | 69 | 1.06 |
| D | | BC 19 | 54 | 0.0844 | 74 | 43 | 0.62 |
| D | | BC 20 | 52 | 0.0813 | 68 | 32 | 0.53 |
| D | | BC 21 | 32 | 0.05 | 64 | 45 | 0.41 |
| D | | BC 22 | 117.65 | 0.1838 | 74 | 85 | 0.5 |
| D | | BC 23 | 54.78 | 0.0856 | 61 | 31 | 0.53 |
| D | | BC 24 | 47.64 | 0.0744 | 61 | 28 | 0.57 |
| D | | BC 25 | 100 | 0.1563 | 61 | 37 | 0.78 |
| D | | BC 26 | 33.2 | 0.0519 | 61 | 42 | 0.49 |
| D | | BC 27 | 26.3 | 0.0411 | 61 | 63 | 0.44 |
| D | | BC 28 | 20.8 | 0.0325 | 61 | 81 | 0.33 |
| D | | BC 29 | 17.7 | 0.0277 | 61 | 80 | 0.39 |
| D | | BC 30 | 52.8 | 0.0825 | 61 | 85 | 0.39 |
| D | | BC 31 | 30.2 | 0.0472 | 72 | 85 | 0.34 |
| D | | BC 32 | 27.5 | 0.043 | 61 | 85 | 0.33 |
| D | | BC 33 | 58 | 0.0906 | 61 | 85 | 0.56 |
| D | | BC 34 | 29 | 0.0453 | 61 | 48 | 0.42 |
| D | | BC 35 | 60 | 0.0938 | 61 | 30 | 0.66 |
| D | | BC 36 | 157 | 0.2453 | 63 | 30 | 0.31 |
| E | West Ave SD Outfall (Watershed E) | WA 1 | 41 | 0.0641 | 61 | 27 | 0.62 |
| E | (Sub-Basins Draining into West Ave Storm Drain) | WA 2 | 54.5 | 0.0852 | 61 | 53 | 0.62 |
| E | | WA 3 | 808 | 0.0138 | 61 | 30 | 0.41 |
| E | | WA 4 | 140 | 0.2188 | 72 | 76 | 0.75 |
| E | | WA 5 | 78.5 | 0.1227 | 67 | 46 | 0.68 |
| E | | WA 6 | 105.6 | 0.165 | 78 | 38 | 0.83 |
| E | | WA 7 | 122.2 | 0.1909 | 63 | 42 | 0.97 |
| E | | WA 8 | 61.5 | 0.0961 | 61 | 58 | 0.71 |

CITY OF MERCED
Storm Drain Master Plan
Hydrologic Parameters Used in HEC-1 Computer Model

Table 1

| Watershed | Outfall | Sub-Basin | Drainage Area (Acres) | Drainage Area (Sq. Mile) | Curve Number | Percent Impervious | Lag Time (hr.) |
|-----------|---|-----------|-----------------------|--------------------------|--------------|--------------------|----------------|
| E | | WA 9 | 35.4 | 0.0553 | 67 | 57 | 0.84 |
| E | | WA 10 | 70.9 | 0.1108 | 71 | 56 | 0.87 |
| E | | WA 11 | 26.6 | 0.0416 | 77 | 73 | 0.58 |
| E | | WA 12 | 9 | 0.0141 | 61 | 83 | 0.27 |
| E | | WA 13 | 26.4 | 0.0413 | 79 | 76 | 0.77 |
| E | | WA 14 | 9 | 0.0141 | 61 | 82 | 0.27 |
| E | | WA 15 | 9.2 | 0.0144 | 80 | 80 | 0.25 |
| E | | WA 16 | 9 | 0.0141 | 65 | 80 | 0.27 |
| E | | WA 17 | 39.3 | 0.0614 | 72 | 81 | 0.43 |
| E | | WA 18 | 18.8 | 0.0294 | 80 | 80 | 0.31 |
| E | | WA 19 | 36.3 | 0.0567 | 80 | 79 | 0.47 |
| E | | WA 20 | 62.2 | 0.0972 | 80 | 82 | 0.6 |
| E | | WA 21 | 46 | 0.0718 | 80 | 65 | 0.55 |
| E | | WA 22 | 38 | 0.0594 | 74 | 25 | 0.91 |
| E | | WA 23 | 123.4 | 0.1928 | 72 | 53 | 0.84 |
| E | | WA 24 | 76.4 | 0.1909 | 61 | 40 | 0.63 |
| E | | WA 25 | 160.6 | 0.2509 | 78 | 34 | 1.04 |
| E | | WA 26 | 35.6 | 0.0556 | 80 | 41 | 0.58 |
| E | | WA 27 | 54 | 0.0844 | 78 | 50 | 0.6 |
| E | | WA 28 | 121 | 0.1891 | 68 | 30 | 1.02 |
| E | | WA 29 | 45.8 | 0.0715 | 63 | 35 | 0.45 |
| F | Zentner Lateral (Watershed F) | ZEN 1 | 40.82 | 0.0638 | 80 | 47 | 0.66 |
| F | (Sub-Basin Draining into Zentner Lateral) | ZEN 2 | 108.64 | 0.1698 | 80 | 42 | 0.83 |
| F | | ZEN 3 | 55.79 | 0.0872 | 75 | 31 | 0.53 |
| F | | ZEN 4 | 44.77 | 0.07 | 73 | 31 | 0.58 |
| F | | ZEN 5 | 90.11 | 0.1408 | 77 | 34 | 0.83 |
| F | | ZEN 6 | 40.58 | 0.0634 | 79 | 85 | 0.49 |
| F | | ZEN 7 | 49.07 | 0.0767 | 73 | 33 | 0.65 |
| F | | ZEN 8 | 76.91 | 0.1202 | 80 | 35 | 0.7 |

CITY OF MERCED
Storm Drain Master Plan
Hydrologic Parameters Used in HEC-1 Computer Model

Table 1

| Watershed | Outfall | Sub-Basin | Drainage Area (Acres) | Drainage Area (Sq. Mile) | Curve Number | Percent Impervious | Lag Time (hr.) |
|-----------|--|-----------|-----------------------|--------------------------|--------------|--------------------|----------------|
| F | | ZEN 9 | 40.86 | 0.0639 | 80 | 56 | 0.63 |
| F | | ZEN 10 | 27.84 | 0.0434 | 80 | 80 | 0.39 |
| F | | ZEN 11 | 32.14 | 0.0502 | 80 | 72 | 0.45 |
| F | | ZEN 12 | 103.31 | 0.1613 | 80 | 30 | 0.93 |
| F | | ZEN 13 | 97 | 0.1516 | 78 | 30 | 0.93 |
| F | | ZEN 14 | 101 | 0.1578 | 76 | 30 | 0.85 |
| F | | ZEN 15 | 38 | 0.0594 | 80 | 27 | 0.61 |
| F | | ZEN 16 | 28.3 | 0.0442 | 80 | 75 | 0.29 |
| F | | ZEN 17 | 68.5 | 0.107 | 80 | 30 | 0.53 |
| F | | ZEN 18 | 118.2 | 0.1847 | 76 | 50 | 0.78 |
| F | | ZEN 19 | 253.3 | 0.3958 | 73 | 33 | 1.43 |
| F | | ZEN 20 | 164 | 0.2563 | 76 | 34 | 0.82 |
| F | | ZEN 21 | 158 | 0.2469 | 77 | 16 | 0.82 |
| F | | ZEN 22 | 59.4 | 0.0928 | 77 | 35 | 0.62 |
| G | Hartley Lateral (Watershed G) | HRL 2 | 307 | 0.4797 | 78 | 37 | 0.78 |
| G | (Sub-Basins Drianing into Hartley Lateral) | HRL 3 | 310 | 0.4844 | 78 | 14 | 1.23 |
| G | | HRL 4 | 50 | 0.0781 | 73 | 50 | 0.52 |
| G | | HRL 4B | 125 | 0.1953 | 80 | 43 | 0.7 |
| G | | HRL 5 | 151 | 0.2359 | 80 | 65 | 0.66 |
| G | | HRL 6 | 294 | 0.4594 | 73 | 59 | 1.13 |
| G | | HRL 7 | 440 | 0.6875 | 73 | 45 | 1.55 |
| H | Doane Canal (Watershed H) | DOA 1 | 480 | 0.75 | 76 | 85 | 1.43 |
| H | (Sub-Basin Draining into Doane Canal) | DOA 2 | 149 | 0.2328 | 78 | 28 | 0.78 |
| H | | DOA 3 | 310 | 0.4844 | 69 | 58 | 1.14 |
| H | | DOA 4 | 640 | 1 | 67 | 85 | 1.33 |
| H | | DOA 5 | 170 | 0.2656 | 72 | 85 | 0.67 |
| I | Farmdale Lateral (Watershed I) | FAR 1 | 166 | 0.2594 | 66 | 34 | 1.03 |
| J | Miles Creek (Watershed J) | MIL 1 | 170 | 0.2656 | 72 | 85 | 0.67 |

CITY OF MERCED
Storm Drain Master Plan
Hydrologic Parameters Used in HEC-1 Computer Model

Table 1

| Watershed | Outfall | Sub-Basin | Drainage Area (Acres) | Drainage Area (Sq. Mile) | Curve Number | Percent Impervious | Lag Time (hr.) |
|------------------|--|------------------|------------------------------|---------------------------------|---------------------|---------------------------|-----------------------|
| K | El Capitan Canal (Watershed K) | ELC 1 | 261 | 0.4078 | 62 | 30 | 0.72 |
| K | (Sub-Basin Draining into EL Capitan Canal) | ELC 2 | 78 | 0.2516 | 70 | 45 | 0.73 |
| K | | ELC 3 | 161 | 0.1219 | 71 | 48 | 0.42 |

Table 2

10-yr Peak Discharges

CITY OF MERCED
Storm Drain Master Plan
10-Year Peak Discharges

Table 2

| Watershed | Sub-Basin | Location of Concentration Point | Drainage Area (Acres) | Drainage Area (Sq. Mile) | 10-Year Discharge (cfs) |
|-----------|-----------|--|--------------------------|--------------------------------|-------------------------------|
| A | FAHR 1 | At Bellevue Rd. Between "G" St & Hwy 59 | 1184 | 1.85 | 238 |
| A | FAHR 2 | At Bellevue Rd. Between "G" St & Hwy 59 | 898 | 1.4031 | 114 |
| A | FAHR 3 | At Bellevue Rd. and Fahrens Creek (CP 1) | 712 | 1.1125 | 94 |
| A | FAHR 4 | At Fahrens Creek & Lehigh Dr. (CP 2) | 595 | 0.9297 | 96 |
| A | FAHR 5 | At Fahrens Creek & Lehigh Dr. (CP 2) | 133 | 0.2078 | 38 |
| A | FAHR 6 | At Fahrens Creek & Yosemite Ave (CP 5) | 207 | 0.3234 | 34 |
| B | COT 1 | At Cottonwood Ck. & Quail Ave (CP 3) | 135 | 0.2109 | 24 |
| B | COT 2 | At Cottonwood Ck. & Quail Ave (CP 3) | 120.64 | 0.1885 | 28 |
| B | COT 3 | At Cottonwood Ck. & "G" St (CP 4) | 151.1 | 0.236 | 28 |
| B | COT 4 | At Cottonwood Ck. & "G" St. (CP 4) | 846.6 | 1.3228 | 127 |
| B | COT 5 | At Cottonwood Ck. E of "G" St (CP 4A) | 266 | 0.4156 | 18 |
| C | BRC 1 | Black Rascal Ck. & Mckee Rd. (CP 8) | 152 | 0.2375 | 30 |
| C | BRC 2 | Black Rascal Ck. & Mckee Rd. (CP 8) | 53.1 | 0.083 | 11 |
| C | BRC 3 | Black Rascal Ck. & Parsons Ave (CP 9) | 94.52 | 0.1477 | 13 |
| C | BRC 4 | At Parsons Ave & El Portal Dr. | 93.55 | 0.1462 | 15 |
| C | BRC 5 | Black Rascal Ck. S of Morain Dome Ct (CP 10) | 57.51 | 0.0899 | 11 |
| C | BRC 6 | Black Rascal Ck. S of Morain Dome Ct (CP 10) | 59.4 | 0.0928 | 12 |
| C | BRC 7 | Black Rascal Ck. S of Morain Dome Ct (CP 10) | 59.97 | 0.0937 | 13 |
| C | BRC 8 | Black Rascal Ck. & Joerg ave (CP 11) | 58.14 | 0.0908 | 12 |
| C | BRC 9 | Black Rascal Ck. & Cherokee Ave (CP 12) | 96.99 | 0.1515 | 17 |
| C | BRC 10 | Black Rascal Ck. & Cordova Ave (CP 13) | 81.44 | 0.1273 | 14 |
| C | BRC 11 | Black Rascal Ck. & Cordova Ave (CP 13) | 90.11 | 0.1408 | 20 |
| C | BRC 12 | Olive Ave & Sycamore Dr. | 20.66 | 0.0323 | 6 |
| C | BRC 13 | Black Rascal Ck. & El Capitan Ct. (CP 14) | 51.31 | 0.0802 | 8 |
| C | BRC 14 | Black Rascal Ck. & "G" St. (CP 15) | 31.34 | 0.049 | 7 |
| C | BRC 14B | Black Rascal Ck. & "G" St. (CP 15) | 49.36 | 0.0771 | 20 |
| C | BRC 15 | At "G" St. and El Portal Dr. | 49.07 | 0.0767 | 14 |
| C | BRC 16 | Black Rascal Ck. & Campus Dr. (CP 16) | 43.9 | 0.0686 | 6 |
| C | BRC 17 | Black Rascal Ck. & "M" St. (CP 17) | 68.01 | 0.1063 | 25 |

CITY OF MERCED
Storm Drain Master Plan
10-Year Peak Discharges

Table 2

| Watershed | Sub-Basin | Location of Concentration Point | Drainage Area (Acres) | Drainage Area (Sq. Mile) | 10-Year Discharge (cfs) |
|-----------|-----------|--|--------------------------|--------------------------------|-------------------------------|
| C | BRC 18 | Black Rascal Ck. & "M" St. (CP 17) | 209.54 | 0.3274 | 43 |
| C | BRC 19 | Black Rascal Ck. BTWN "M" St & "R" St. (CP 18) | 44 | 0.0688 | 8 |
| C | BRC 20 | Black Rascal Ck. BTWN "M" St & "R" St. (CP 19) | 85 | 0.1328 | 20 |
| C | BRC 21 | Black Rascal Ck. BTWN "M" St & "R" St (CP 19) | 116.79 | 0.1825 | 56 |
| C | BRC 22 | Black Rascal Ck. West of "R" St (CP 20) | 104.91 | 0.1639 | 25 |
| C | BRC 23 | Black Rascal Ck. & Chyanne Dr. (CP 21) | 212.75 | 0.3324 | 34 |
| C | BRC 24 | Hwy 59 & Cardella Rd. (CP 22) | 706 | 1.1031 | 155 |
| C | BRC 25 | Hwy 59 & Belcher Ave. (CP 23) | 380 | 0.5938 | 108 |
| C | BRC 26 | Hwy 59 & Black Rascal Ck. (CP 7) | 376 | 0.5875 | 88 |
| C | BRC 27 | Black Rascal Ck. & Santa Fee Railroad (CP 24) | 621 | 0.9703 | 202 |
| C | BRC 28 | Black Rascal Ck. & Santa Fee Railroad (CP 24) | 32.43 | 0.0507 | 19 |
| C | BRC 29 | Black Rascal Ck. & El Capitan Canal. (CP 25) | 188.13 | 0.294 | 70 |
| C | BRC 30 | Flood Channel East of Hwy 59 | 142 | 0.2219 | 42 |
| C | BRC 31 | Black Rascal Ck. & Hwy 59 (CP 7) | 78 | 0.1219 | 19 |
| D | BC 1 | Bear Ck. BTWN Mckee Rd & Bedford Ln (CP 26) | 92 | 0.1438 | 15 |
| D | BC 2 | Bear Ck. & Bedford Ln (CP 27) | 37.02 | 0.0578 | 10 |
| D | BC 3 | Bear Ck. & Bedford Ln (CP 27) | 87.81 | 0.1372 | 14 |
| D | BC 4 | Santa Fee Ave & Green St. | 156 | 0.2438 | 28 |
| D | BC 5 | Midge Ave south of East 27th St (CP 29) | 74.04 | 0.1157 | 14 |
| D | BC 6 | Midge Ave & East 27th St (CP 30) | 18.37 | 0.0287 | 4 |
| D | BC 7 | Midge Ave & East 27th St (CP 30) | 48.78 | 0.0762 | 6 |
| D | BC 8 | Bear Ck. & Cameron Ln. (CP 28) | 54.64 | 0.0854 | 8 |
| D | BC 9 | Bear Ck. & Cameron Ln. (CP 28) | 139.18 | 0.2175 | 22 |
| D | BC 10 | Bear Ck. & Wainwright Ave (CP 31) | 83.16 | 0.1299 | 18 |
| D | BC 11 | Near Parsons Ave & Oregon Dr. (CP 33) | 11.48 | 0.0179 | 4 |
| D | BC 12 | Near Hensons Ave & Nottingham Ln (CP 34) | 42.47 | 0.0664 | 9 |
| D | BC 13 | "G" Street & Craig Dr. (CP 35) | 97.57 | 0.1525 | 16 |
| D | BC 14 | Bear Creek & "M" Street (CP 36) | 149.28 | 0.2333 | 47 |
| D | BC 15 | Bear Creek & Ardell Dr. (CP 37) | 18.5 | 0.0289 | 4 |

CITY OF MERCED
Storm Drain Master Plan
10-Year Peak Discharges

Table 2

| Watershed | Sub-Basin | Location of Concentration Point | Drainage Area (Acres) | Drainage Area (Sq. Mile) | 10-Year Discharge (cfs) |
|-----------|-----------|--|-----------------------|--------------------------|-------------------------|
| D | BC 16 | Bear Creek & "R" Street (CP 38) | 37.5 | 0.0586 | 7 |
| D | BC 17 | Bear Creek Near W 25th & "V" Street (CP 39) | 30.42 | 0.0475 | 6 |
| D | BC 18 | Bear Creek @ Santa Fe Railroad (CP 40) | 173 | 0.2703 | 51 |
| D | BC 19 | Bear Creek Near Creekside Dr. (CP 41) | 54 | 0.0844 | 14 |
| D | BC 20 | Bear Creek Near Brookside Dr. (CP 42) | 52 | 0.0813 | 10 |
| D | BC 21 | Bear Creek Near West 16th Street (CP 43) | 32 | 0.05 | 10 |
| D | BC 22 | Bear Creek @ Auto Center SD Pump Station (CP 44) | 117.65 | 0.1838 | 63 |
| D | BC 23 | 22nd Street & "T" Street (CP 45) | 54.78 | 0.0856 | 10 |
| D | BC 24 | 20th Street & "T" Street & (CP 46) | 47.64 | 0.0744 | 8 |
| D | BC 25 | 22nd Street & "S" Street (CP 47) | 100 | 0.1563 | 19 |
| D | BC 26 | 18th Street & "T" Street (CP 48) | 33.2 | 0.0519 | 9 |
| D | BC 27 | 18th Street & "R" Street (CP 49) | 26.3 | 0.0411 | 11 |
| D | BC 28 | 16th Street & "T" St (CP 50) | 20.8 | 0.0325 | 12 |
| D | BC 29 | 16th Street & "Q" Street (CP 51) | 17.7 | 0.0277 | 10 |
| D | BC 30 | 16th Street & "U" Street (CP 52) | 52.8 | 0.0825 | 31 |
| D | BC 31 | 15th Street & "R" Street (CP 54) | 30.2 | 0.0472 | 19 |
| D | BC 32 | 15th Street & "U" Street (CP 53) | 27.5 | 0.043 | 17 |
| D | BC 33 | Auto Center Storm Drain Pump Station (CP 44) | 58 | 0.0906 | 29 |
| D | BC 34 | Griffin Street and Bear Creek | 29 | 0.0453 | 9 |
| D | BC 35 | Massasso Street and Bear Creek | 60 | 0.0938 | 10 |
| D | BC 36 | Massasso Street and Bear Creek | 157 | 0.2453 | 35 |
| E | WA 1 | Lopes Ave & West Ave (CP 55) | 41 | 0.0641 | 6 |
| E | WA 2 | 18th Street & West Ave (CP 55) | 54.5 | 0.0852 | 16 |
| E | WA 3 | Wardrobe Ave & West Ave (CP 56) | 8.8 | 0.0138 | 2 |
| E | WA 4 | Grogan Ave & West Ave (CP 57) | 140 | 0.2188 | 55 |
| E | WA 5 | 19th Ave & "U" Street (CP 59) | 78.5 | 0.1227 | 20 |
| E | WA 6 | Grogan Ave & West Ave (CP 57) | 105.6 | 0.165 | 25 |
| E | WA 7 | 23rd Street & "M" Street (CP 60) | 122.2 | 0.1909 | 23 |
| E | WA 8 | 23rd Street & "O" Street (CP 61) | 61.5 | 0.0961 | 19 |

CITY OF MERCED
Storm Drain Master Plan
10-Year Peak Discharges

Table 2

| Watershed | Sub-Basin | Location of Concentration Point | Drainage Area (Acres) | Drainage Area (Sq. Mile) | 10-Year Discharge (cfs) |
|-----------|-----------|---|-----------------------|--------------------------|-------------------------|
| E | WA 9 | 22nd Street & "O" Street (CP 62) | 35.4 | 0.0553 | 10 |
| E | WA 10 | 20th Street & "O" Street & (CP 63) | 70.9 | 0.1108 | 19 |
| E | WA 11 | 19th Street & "M" Street (CP 64) | 26.6 | 0.0416 | 12 |
| E | WA 12 | 19th Street & "O" Street (CP 65) | 9 | 0.0141 | 6 |
| E | WA 13 | 18th Street & "M" Street (CP 66) | 26.4 | 0.0413 | 11 |
| E | WA 14 | 18th Street & "O" Street (CP 67) | 9 | 0.0141 | 6 |
| E | WA 15 | Main Street & "M" Street (CP 68) | 9.2 | 0.0144 | 6 |
| E | WA 16 | Main Street & "O" Street (CP 69) | 9 | 0.0141 | 6 |
| E | WA 17 | 16th Street & "O" Street (CP 70) | 39.3 | 0.0614 | 21 |
| E | WA 18 | 16th Street & MLK Way (CP 72) | 18.8 | 0.0294 | 12 |
| E | WA 19 | 13th Street & MLK Way (CP 73) | 36.3 | 0.0567 | 19 |
| E | WA 20 | 13th Street & "O" Street (CP 71) | 62.2 | 0.0972 | 31 |
| E | WA 21 | 11th Street & "O" Street (CP 74) | 46 | 0.0718 | 20 |
| E | WA 22 | Childs Ave & "O" Street (CP 75) | 38 | 0.0594 | 6 |
| E | WA 23 | Childs Ave & "N" Street (CP 76) | 123.4 | 0.1928 | 33 |
| E | WA 24 | Childs Ave & "N" Street (CP 76) | 76.4 | 0.1909 | 27 |
| E | WA 25 | Childs Ave & "R" Street (CP 77) | 160.6 | 0.2509 | 31 |
| E | WA 26 | Childs Ave & West Ave (CP 58) | 35.6 | 0.0556 | 11 |
| E | WA 27 | Riggs Road & West Ave (CP 78) | 54 | 0.0844 | 18 |
| E | WA 28 | Gerard Ave & West Ave (CP 79) | 121 | 0.1891 | 16 |
| E | WA 29 | "N" Street south of Childs Ave | 45.8 | 0.0715 | 10 |
| F | ZEN 1 | Anderegg Ave & Yosemite Parkway (CP 80) | 40.82 | 0.0638 | 15 |
| F | ZEN 2 | Union Ave & Yosemite Parkwy (CP 81) | 108.64 | 0.1698 | 29 |
| F | ZEN 3 | Glen Ave & 21th Street (CP 82) | 55.79 | 0.0872 | 13 |
| F | ZEN 4 | Glen Ave & Yomemite Parkway (CP 83) | 44.77 | 0.07 | 9 |
| F | ZEN 5 | Main Street & "D" Street (CP 84) | 90.11 | 0.1408 | 19 |
| F | ZEN 6 | 15th Street & "G" Street (CP 85) | 40.58 | 0.0634 | 22 |
| F | ZEN 7 | Santa Fee Ave & "G" Street (CP 86) | 49.07 | 0.0767 | 10 |
| F | ZEN 8 | 20th Street & "G" Street (CP 87) | 76.91 | 0.1202 | 20 |

CITY OF MERCED
Storm Drain Master Plan
10-Year Peak Discharges

Table 2

| Watershed | Sub-Basin | Location of Concentration Point | Drainage Area (Acres) | Drainage Area (Sq. Mile) | 10-Year Discharge (cfs) |
|-----------|-----------|---|-----------------------|--------------------------|-------------------------|
| F | ZEN 9 | 15th Street & "G" Street (CP 85) | 40.86 | 0.0639 | 15 |
| F | ZEN 10 | 16th Street & "G" Street (CP 88) | 27.84 | 0.0434 | 16 |
| F | ZEN 11 | 11th Street & "G" Street (CP 89) | 32.14 | 0.0502 | 16 |
| F | ZEN 12 | Childs Ave & "G" Street (CP 90) | 103.31 | 0.1613 | 22 |
| F | ZEN 13 | Cone Ave East of South "G" Street (CP 91) | 97 | 0.1516 | 19 |
| F | ZEN 14 | South "G" Street BTWN Cone Ave & Gerard Ave (CP 92) | 101 | 0.1578 | 19 |
| F | ZEN 15 | West of (CP 92) @ (CP 93) | 38 | 0.0594 | 9 |
| F | ZEN 16 | 11th Street & MLK Way | 28.3 | 0.0442 | 17 |
| F | ZEN 17 | Childs Ave & MLK Way (CP 95) | 68.5 | 0.107 | 19 |
| F | ZEN 18 | Gerard Ave BTWN "N" & "P" Street (CP 96) | 118.2 | 0.1847 | 33 |
| F | ZEN 19 | Mission Ave & Hwy 59 (CP 97) | 253.3 | 0.3958 | 35 |
| F | ZEN 20 | Dickenson Ferry Rd. BTWN Hwy 59 & West Ave (CP 98) | 164 | 0.2563 | 34 |
| F | ZEN 21 | Dickenson Ferry Rd. & West Ave (CP 99) | 158 | 0.2469 | 22 |
| F | ZEN 22 | Gerard Ave East of Hwy 59 (CP 4) | 59.4 | 0.0928 | 15 |
| G | HRL 2 | Parsons Ave & Dinkey Ck Ave (CP 100) | 307 | 0.4797 | 73 |
| G | HRL 3 | Childs Ave & Parsons Ave | 310 | 0.4844 | 58 |
| G | HRL 4 | Childs Ave & Carol Ave | 50 | 0.0781 | 16 |
| G | HRL 4B | Merced Ave & I-99 | 125 | 0.1953 | 37 |
| G | HRL 5 | Childs Ave & Tyler Road (CP 101) | 151 | 0.2359 | 62 |
| G | HRL 6 | Gerard Ave & Tyler Road (CP 102) | 294 | 0.4594 | 75 |
| G | HRL 7 | Mission Ave & Tyler Road (CP103) | 440 | 0.6875 | 75 |
| H | DOA 1 | Childs Ave & Doane Canal (CP 104) | 480 | 0.75 | 151 |
| H | DOA 2 | Childs Ave & Doane Canal (CP 104) | 149 | 0.2328 | 30 |
| H | DOA 3 | Mission Ave & Doane Canal (CP 105) | 310 | 0.4844 | 75 |
| H | DOA 4 | Mission Ave & Doane Canal (CP 105) | 640 | 1 | 205 |
| H | DOA 5 | Doane Canal & Miles Creek | 170 | 0.2656 | 79 |
| I | HRL 1 | Mission Ave & Alfarata Blvd | 166 | 0.2594 | 25 |
| G | MIL 1 | Miles Creek | 170 | 0.2656 | 79 |

CITY OF MERCED
Storm Drain Master Plan
10-Year Peak Discharges

Table 2

| Watershed | Sub-Basin | Location of Concentration Point | Drainage Area (Acres) | Drainage Area (Sq. Mile) | 10-Year Discharge (cfs) |
|-----------|-----------|------------------------------------|--------------------------|--------------------------------|-------------------------------|
| K | ELC 1 | McSwain Rd (I-140) & Thornton Rd | 261 | 0.4078 | 41 |
| K | ELC 2 | Lopes Ave BTWN East of Thornton Rd | 161 | 0.2516 | 39 |
| K | ELC 3 | Lopes Ave & Thornton Rd | 78 | 0.1219 | 26 |

Table 3

Hydrologic Parameters Used in HEC-1 Model

CITY OF MERCED
Storm Drain Master Plan
Proposed Detention Basin Data

Table 3

| Detention Basins | Location | Surface Area (Ac) | 50-Year Inflow (cfs) | 2-Year * Outflow (cfs) | Storage Volume (Ac-Ft) | Depth of Water (ft) | Freeboard (ft) |
|------------------|-------------------------------------|-------------------|----------------------|------------------------|------------------------|---------------------|----------------|
| 1 | At Bellevue Rd BTWN "G" St & Hwy 59 | 45 | 522 | 34 | 257 | 5.9 | 1 |
| 2 | At Bellevue Rd BTWN "G" St & Hwy 59 | 20 | 143 | 9 | 73 | 3.8 | 1 |
| 3 | At Cottonwood Ck & "G" St | 25 | 197 | 12 | 95 | 3.9 | 1 |
| 4 | Near Fahrens Ck & Lehigh Dr | 18 | 147 | 9 | 62 | 3.6 | 1 |
| 5 | At Belcher Ave & Hwy 59 | 37 | 366 | 25 | 149 | 4.1 | 1 |
| 6 | Hwy 59 & Black Rascal Creek | 20 | 155 | 9 | 84 | 4.3 | 1 |
| 7 | Black Rascal Ck & Santa Fe Railroad | 27 | 274 | 21 | 102 | 3.9 | 1 |
| 8 | Dickenson Ferry Rd & West Ave | 45 | 589 | 43 | 188 | 4.3 | 1 |
| 9 | Cone Ave & South "G" St | 25 | 306 | 19 | 97 | 3.8 | 1 |
| 10 | MLK Way & Childs Ave | 3 | 52 | 4 | 10 | 3.7 | 1 |
| 11 | Gerard Ave east of Hwy 59 | 5 | 49 | 7 | 16 | 3.4 | 1 |
| 12 | Mission Ave BTWN West Ave & Hwy 59 | 13 | 96 | 7 | 42 | 3.6 | 1 |
| 13 | Parsons Ave & Dinkey Ck Ave | 20 | 169 | 11 | 69 | 3.6 | 1 |
| 14 | Childs Ave & Tyler Road | 10 | 140 | 8 | 38 | 3.9 | 1 |
| 15 | Gerard Ave & Tyler Road | 10 | 106 | 8 | 38 | 3.9 | 1 |
| 16 | Mission Ave & Tyler Road | 13 | 111 | 8 | 50 | 4 | 1 |
| 17 | Childs Ave & Doane Canal | 25 | 241 | 16 | 97 | 4 | 1 |
| 18 | Mission Ave & Doane Canal | 37 | 380 | 24 | 146 | 4.1 | 1 |
| 19 | Vassar Ave & Doane Canal | 7 | 107 | 8 | 25 | 3.8 | 1 |
| 20 | Mission Ave & Alfarata Blvd | 3 | 36 | 5 | 11 | 3.9 | 1 |
| 21 | Vassar Ave BTWN Henry St & I-99 | 7 | 107 | 8 | 25 | 3.8 | 1 |
| 22 | McSwain Rd (I-140) & Thornton Rd | 5 | 56 | 4 | 18 | 3.9 | 1 |

* Outflow is approximately equal to 2-year storm discharge under existing conditions.

Table 4

Cost Estimate for Proposed Pump Stations

CITY OF MERCED
Storm Drain Master Plan
General Cost Estimates for Pump Stations of Varying Capacities

Table 4

| Input Data | | | | | Costs | | | | | |
|---------------------|------------|--------------------|----------------|---------------------|----------------|----------------------|----------------------|----------------------|-------------------|------------|
| Max Flow Rate (cfs) | # of Pumps | Flow Rate per Pump | Pump Size (hp) | Discharge Pipe Size | Pump Equipment | Mechanical Equipment | Electrical Equipment | Structural/ Building | Site Improvements | Total |
| 5 | 3 | 2.5 | 9.5 | 12" | \$ 100,000 | \$ 40,000 | \$ 50,000 | \$ 50,000 | \$ 40,000 | \$ 280,000 |
| 10 | 3 | 5 | 18.9 | 16" | \$ 100,000 | \$ 50,000 | \$ 60,000 | \$ 60,000 | \$ 40,000 | \$ 310,000 |
| 15 | 3 | 7.5 | 28.4 | 20" | \$ 100,000 | \$ 60,000 | \$ 65,000 | \$ 65,000 | \$ 40,000 | \$ 330,000 |
| 20 | 3 | 10 | 37.8 | 24" | \$ 100,000 | \$ 70,000 | \$ 70,000 | \$ 70,000 | \$ 60,000 | \$ 370,000 |
| 30 | 3 | 15 | 56.7 | 30" | \$ 225,000 | \$ 100,000 | \$ 75,000 | \$ 75,000 | \$ 60,000 | \$ 535,000 |
| 40 | 3 | 20 | 75.6 | 30" | \$ 260,000 | \$ 100,000 | \$ 100,000 | \$ 100,000 | \$ 60,000 | \$ 620,000 |

Table 5

Existing Stormwater Storage Facilities

CITY OF MERCED
Storm Drain Master Plan
Existing Stormwater Storage Facilities

Table 5

| Fund # | Station # | Detention Type | Location | Storage Vol. (cf) | Storage Vol. (af) | SDMP Sub-Basins | 10-Year Vol. (af) | 50-Year Vol. (af) |
|---------------|------------------|-----------------------|----------------------|--------------------------|--------------------------|------------------------|--------------------------|--------------------------|
| 101 | 31 | Pipe & Pump Station | 1590 Massasso St | 97,000 | 2.22 | BC 35 | 3 | 5 |
| 106 | 18 | Pond & Pump Station | 1813 Lopes Ave | 150,000 | 3.44 | WA 1 | 2 | 3 |
| 107 | 35 | Pipe | 3092 Queens Cr | 66,300 | 1.50 | BRC 12 | 2 | 3 |
| 108 | 16 | Pond & Pump Station | 1425 W.N Beer Ck | 95,000 | 2.18 | BC 19 | 5 | 7 |
| 109 | 19 | Pond & Pump Station | 71 E. Gerard Ave | 217,800 | 5.00 | ZEN 14 | 8 | 12 |
| 110 | 21 | Pond & Pump Station | 986 Auburn Ct | 280,000 | 6.43 | FAHR6 | 15 | 23 |
| 111 | 24 | Pond & Pump Station | 2090 Lopes Ave | 260,000 | 5.97 | ELC 2 | 14 | 21 |
| 113 | 22 | Pond | 912 W. Donna Dr | 65,000 | 1.50 | BRC19 | 3 | 5 |
| 116 | 30 | Pipe | 3505 Paulson Dr | 26,000 | 0.60 | BRC 9 | 7 | 11 |
| 117 | 27 | Pond & Pump Station | Auto Center Dr | 55,000 | 1.26 | Auto Center | 48 | 66 |
| 118 | 38 | Pipe | 5 Cormorant Dr | 250,000 | 5.74 | COT 1 | 10 | 15 |
| 121 | 11 | Pipe & Pump Station | 100 Parsons Ave | 90,000 | 2.07 | HRL 2 | 28 | 41 |
| 122 | 6 | no storage added | 1150 Paseo Verde Dr | N A | N A | BRC 22 | 8 | 13 |
| 124 | 4 | Private Ret | 1317 W.E. Beer Ck | 20,000 | 0.46 | BC 18 | 21 | 28 |
| 125 | 2 | Pond & Pump Station | 100 Campus Dr | 125,000 | 2.87 | BRC 18 | 17 | 26 |
| 127 | 20 | Pond | 1510 hansen Ave | 52,000 | 1.19 | BC 12 | 3 | 5 |
| 102/114 | 40 | Pond | 1200 E. El Portal Dr | 387,000 | 8.88 | BRC 6 | 4 | 7 |

Table 6

Existing Stormwater Pump Stations

CITY OF MERCED
Storm Drain Master Plan
Existing Stormwater Pump Stations

Table 6

| Station # | Location | Number of Pumps | Pumping Capacity (gpm) | Total Capacity (gpm) | Pumping Capacity (cfs) | SDMP Sub-basins | 10-Year Discharges (cfs) |
|-----------|------------------------|-----------------|------------------------|----------------------|------------------------|-------------------------|--------------------------|
| 1 | Flamingo & West Ave | 2 | 1 @ 5500 1 @ 1500 | 7000 | 15.60 | West Ave Storm Drain ** | 405 |
| 2 | Campus North | 3 | 3000 ea | 9000 | 20.05 | BRC 18 (campus Dr) | 43 |
| 3* | Cooper Ave | 3 | 2 @ 15000 1 @ 3000 | 33000 | 73.52 | BRC 29 | 70 |
| 4 | Bear Ck (Olivewood II) | 2 | 8000 ea | 16000 | 35.65 | BC 18 | 51 |
| 5* | Bismark | 2 | 1 @ 11500 1 @ 2200 | 13700 | 30.52 | BRC 23 | 34 |
| 6 | Fahrans Park | 3 | 3000 ea | 9000 | 20.05 | BRC 22 | 25 |
| 7* | Parsons & Hansen Ave | | no data | no data | no data | BC 11 | 4 |
| 9* | Cameron Lane | 2 | 1 @ 3000 1 @ 1000 | 4000 | 8.91 | BC 4, 5, 6, 7 & 8 | 57 |
| 11 | Childs & Parsons | 2 | 1 @ 800 1 @ 1000 | 1800 | 4.01 | HRL 2 | 73 |
| 16 | Sunset | 2 | 2450 ea | 4900 | 10.92 | BC 19 | 14 |
| 18 | Lopes Ave | 2 | 485 ea | 970 | 2.20 | WA1 | 6 |
| 19 | Gerard Ave | 2 | 320 ea | 640 | 1.42 | ZEN14 | 19 |
| 21 | Auburn Ct | 2 | 2400 ea | 4800 | 10.69 | FAHR 6 | 34 |
| 23* | 1368 Griffin Street | | no data | no data | no data | BC 34 | 9 |
| 24 | Lopes Ave | 2 | 485 ea | 970 | 2.20 | ELC2 | 39 |
| 25* | 1801 Wardrobe Ave | | no data | no data | no data | WA 1 | 6 |
| 27 | Auto Center Dr | 3 | 3000 ea | 9000 | 20.05 | Auto Center Storm Drain | 160 |
| 31 | Massasso | 2 | 800 ea | 1600 | 3.56 | BC 35 | 10 |
| 35 | 3092 Queens Circle | | no data | no data | no data | BRC 12 | 6 |
| 38 | Tanager & Cormorant | 2 | 3000 ea | 6000 | 13.37 | COT 1 | 24 |
| 40 | Rahilly Park | 2 | 5000 ea | 10000 | 22.28 | BRC 6 & BRC 8 | 24 |

* Stations outside of Maintenance Districts

** Station pumps water into MID Canal

Table 7

Cost Estimate

CITY OF MERCED
Storm Drain Master Plan
Drainage Infrastructure Required to Serve Areas Draining Into Fahrens Creek
Cost Estimate

Table 7

Watershed A

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|-----------------|-------------|------------------|----------------------|
| <u>Detention Basins</u> | | | | |
| (Onsite Detention Basins 1, 2 & 4) | 447 | AF | 10,000 | 4,470,000 |
| <u>Pump Stations</u> | | | | |
| Detention Basin 1 | 1 | LS | 578,000 | 578,000 |
| Detention Basin 2 | 1 | LS | 310,000 | 310,000 |
| Detention Basin 4 | 1 | LS | 310,000 | 310,000 |
| <u>Channel</u> | | | | |
| 60' R/W | 5,200 | LF | 50 | 260,000 |
| <u>Storm Drain</u> | | | | |
| 30" SD | 8,707 | LF | 80 | 696,560 |
| 36" SD | 2,547 | LF | 100 | 254,700 |
| 42" SD | 18,020 | LF | 120 | 2,162,400 |
| 48" SD | 1,812 | LF | 130 | 235,560 |
| 54" SD | 2,639 | LF | 140 | 369,460 |
| 60" SD | 5,300 | LF | 160 | 848,000 |
| 66" SD | 1,383 | LF | 200 | 276,600 |
| <u>Subtotal Construction</u> | | | | 10,771,280 |
| <u>Design & Planning @ 10%</u> | | | | 1,077,128 |
| <u>Construction Management @10%</u> | | | | 1,077,128 |
| <u>Land Acquisition</u> | | | | |
| Detention Basins 1, 2 & 4 | 83 | AC | 3,500 | 290,500 |
| Channel | 7 | AC | 3,500 | 24,850 |
| <u>Contingency @ 15%</u> | | | | 1,615,692 |
| <u>Program Implementation @ 5%</u> | | | | 538,564 |
| <u>TOTAL ESTIMATED COST</u> | | | | \$ 15,395,142 |

CITY OF MERCED
Storm Drain Master Plan

Drainage Infrastructure Required to Serve Areas Draining Into Cottonwood Creek
Cost Estimate

Table 7

Watershed B

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|-----------------|-------------|------------------|---------------------|
| <u>Detention Basin</u> | | | | |
| (Onsite Detention Basin 3) | 122 | AF | 10,000 | 1,220,000 |
| <u>Pump Station</u> | | | | |
| Detention Basin 3 | 1 | LS | 330,000 | 330,000 |
| <u>Storm Drain</u> | | | | |
| 30" SD | 5,089 | LF | 80 | 407,120 |
| 36" SD | 1,914 | LF | 100 | 191,400 |
| 48" SD | 1,646 | LF | 130 | 213,980 |
| 54" SD | 1,339 | LF | 140 | 187,460 |
| 60" SD | 1,804 | LF | 160 | 288,640 |
| <u>Subtotal Construction</u> | | | | 2,838,600 |
| <u>Design & Planning @ 10%</u> | | | | 283,860 |
| <u>Construction Management @10%</u> | | | | 283,860 |
| <u>Land Acquisition</u> | | | | |
| Detention Basin 3 | 25 | AC | 3,500 | 87,500 |
| <u>Contingency @ 15%</u> | | | | 425,790 |
| <u>Program Implementation @ 5%</u> | | | | 141,930 |
| <u>TOTAL ESTIMATED COST</u> | | | | \$ 4,061,540 |

CITY OF MERCED
Storm Drain Master Plan

Drainage Infrastructure Required to Serve Areas Draining Into Black Rascal Ck.
Cost Estimate

Table 7

Watershed C

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|-----------------|-------------|------------------|----------------------|
| <u>Detention Basins</u> | | | | |
| (Onsite Detention Basins 5, 6 & 7) | 409 | AF | 10,000 | 4,090,000 |
| <u>Pump Stations</u> | | | | |
| Detention Basin 5 | 1 | LS | 453,000 | 453,000 |
| Detention Basin 6 | 1 | LS | 310,000 | 310,000 |
| Detention Basin 7 | 1 | LS | 390,000 | 390,000 |
| <u>Storm Drain</u> | | | | |
| 36" SD | 4,065 | LF | 100 | 406,500 |
| 42" SD | 6,125 | LF | 120 | 735,000 |
| 48" SD | 4,803 | LF | 130 | 624,390 |
| 54" SD | 6,658 | LF | 140 | 932,120 |
| 60" SD | 10,491 | LF | 160 | 1,678,560 |
| <u>Subtotal Construction</u> | | | | 9,619,570 |
| <u>Design & Planning @ 10%</u> | | | | 961,957 |
| <u>Construction Management @10%</u> | | | | 961,957 |
| <u>Land Acquisition</u> | | | | |
| Detention Basins 5, 6 & 7 | 82 | AC | 3,500 | 287,000 |
| <u>Contingency @ 15%</u> | | | | 1,442,936 |
| <u>Program Implementation @ 5%</u> | | | | 480,979 |
| <u>TOTAL ESTIMATED COST</u> | | | | \$ 13,754,398 |

CITY OF MERCED
Storm Drain Master Plan
 Drainage Infrastructure Required to Serve Areas Draining Into Bear Creek
Cost Estimate

Table 7

Watershed D

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|-----------------|-------------|------------------|-------------------|
| <u>Pump Station</u> | | | | |
| Upgrade Auto Center Dr. Pump Station | 1 | LS | 705,000 | 705,000 |
| <u>Storm Drain</u> | | | | |
| 30" SD | 4,448 | LF | 80 | 355,840 |
| 36" SD | 1,822 | LF | 100 | 182,200 |
| 42" SD | 1,396 | LF | 120 | 167,520 |
| 48" SD | 1,879 | LF | 130 | 244,270 |
| 72" SD | 1,415 | LF | 240 | 339,600 |
| 78" SD | 2,106 | LF | 300 | 631,800 |
| 1-48" RCP (Jack & Bore At SPRR) | 100 | LF | 700 | 70,000 |
| <u>Subtotal Construction</u> | | | | 2,696,230 |
| <u>Design & Planning @ 10%</u> | | | | 269,623 |
| <u>Construction Management @10%</u> | | | | 269,623 |
| <u>Contingency @ 15%</u> | | | | 404,435 |
| <u>Program Implementation @ 5%</u> | | | | 134,812 |
| <u>TOTAL ESTIMATED COST</u> | | | \$ | 3,774,722 |

CITY OF MERCED
Storm Drain Master Plan

Drainage Infrastructure Required to Serve Areas Draining Into West Ave Storm Drain
Cost Estimate

Table 7

Watershed E

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|-----------------|-------------|------------------|-------------------|
| <u>Detention Basin</u> | | | | |
| (Detention Basin 8) | 220 | AF | 10,000 | 2,200,000 |
| <u>Pump Station</u> | | | | |
| Detention Basin 8 | 1 | LS | 630,000 | 630,000 |
| <u>Storm Drains/Culverts</u> | | | | |
| 24" SD | 2,225 | LF | 60 | 133,500 |
| 30" SD | 13,694 | LF | 80 | 1,095,520 |
| 36" SD | 8,725 | LF | 100 | 872,500 |
| 42" SD | 4,451 | LF | 120 | 534,120 |
| 48" SD | 390 | LF | 130 | 50,700 |
| 72" SD | 3,457 | LF | 240 | 829,680 |
| 78" SD | 4,344 | LF | 300 | 1,303,200 |
| 1-30" RCP (Jack & Bore At SPRR) | 100 | LF | 500 | 50,000 |
| New 2-10'x4' RCB (airport runway) | 1,600 | LF | 400 | 640,000 |
| Add 1-6'x4' RCB (Dickenson Ferry Rd.) | 1 | LS | 35,000 | 35,000 |
| New 2-60" RCP (Hartley Slough Crossing) | 100 | LF | 160 | 16,000 |
| <u>Channel Improvement</u> | | | | |
| City Storm Drain Channel | 2,800 | LF | 5 | 14,000 |
| <u>Subtotal Construction</u> | | | | 8,404,220 |
| <u>Design & Planning @ 10%</u> | | | | 840,422 |
| <u>Construction Management @10%</u> | | | | 840,422 |
| <u>Land Acquisition</u> | | | | |
| Detention Basin 8 | 45 | AC | 3,500 | 157,500 |
| <u>Contingency @ 15%</u> | | | | 1,260,633 |
| <u>Program Implementation @ 5%</u> | | | | 420,211 |
| <u>TOTAL ESTIMATED COST</u> | | | \$ | 11,923,408 |

CITY OF MERCED
Storm Drain Master Plan

Drainage Infrastructure Required to Serve Areas Draining Into Zentner Lateral Canal
Cost Estimate

Table 7

Watershed F

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|-----------------|-------------|------------------|---------------------|
| Detention Basins | | | | |
| (Detention Basins 9, 10, 11 & 12) | 221 | AF | 10,000 | 2,210,000 |
| Pump Stations | | | | |
| Detention Basin 9 | 1 | LS | 370,000 | 370,000 |
| Detention Basin 10 | 1 | LS | 280,000 | 280,000 |
| Detention Basin 11 | 1 | LS | 280,000 | 280,000 |
| Detention Basin 12 | 1 | LS | 310,000 | 310,000 |
| Storm Drains | | | | |
| 24" SD | 6,588 | LF | 60 | 395,280 |
| 30" SD | 11,730 | LF | 80 | 938,400 |
| 36" SD | 2,592 | LF | 100 | 259,200 |
| 42" SD | 4,229 | LF | 120 | 507,480 |
| 48" SD | 2,195 | LF | 130 | 285,350 |
| 54" SD | 1,836 | LF | 140 | 257,040 |
| 60" SD | 1,100 | LF | 160 | 176,000 |
| 66" SD | 890 | LF | 200 | 178,000 |
| 1-30" RCP (Jack & Bore At Santa Fe RR) | 100 | LF | 500 | 50,000 |
| 1-48" RCP (Jack & Bore at SPRR) | 100 | LF | 700 | 70,000 |
| <u>Subtotal Construction</u> | | | | 6,566,750 |
| <u>Design & Planning @ 10%</u> | | | | 656,675 |
| <u>Construction Management @10%</u> | | | | 656,675 |
| <u>Land Acquisition</u> | | | | |
| Detention Basin 9, 10, 11 & 12 | 46 | AC | 3,500 | 161,000 |
| <u>Contingency @ 15%</u> | | | | 985,013 |
| <u>Program Implementation @ 5%</u> | | | | 328,338 |
| <u>TOTAL ESTIMATED COST</u> | | | | \$ 9,354,450 |

CITY OF MERCED
Storm Drain Master Plan

Drainage Infrastructure Required to Serve Areas Draining Into Hartley Lateral Canal
Cost Estimate

Table 7

Watershed G

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|----------|------|-----------|----------------------|
| <u>Detention Basins</u> | | | | |
| (Detention Basins 13, 14, 15 & 16) | 255 | AF | 10,000 | 2,550,000 |
| | | | | |
| <u>Pump Stations</u> | | | | |
| Detention basin 13 | 1 | LS | 330,000 | 330,000 |
| Detention basin 14 | 1 | LS | 310,000 | 310,000 |
| Detention basin 15 | 1 | LS | 310,000 | 310,000 |
| Detention basin 16 | 1 | LS | 310,000 | 310,000 |
| | | | | |
| <u>Storm Drain</u> | | | | |
| 30" SD | 12,018 | LF | 80 | 961,440 |
| 36" SD | 7,212 | LF | 100 | 721,200 |
| 42" SD | 5,330 | LF | 120 | 639,600 |
| 48" SD | 4,468 | LF | 130 | 580,840 |
| 54" SD | 2,589 | LF | 140 | 362,460 |
| 1-48" RCP (Jack & Bore I-99) | 200 | LF | 700 | 140,000 |
| <u>Subtotal Construction</u> | | | | 7,215,540 |
| <u>Design & Planning @ 10%</u> | | | | 721,554 |
| <u>Construction Management @10%</u> | | | | 721,554 |
| | | | | |
| <u>Land Acquisition</u> | | | | |
| Detention Basins 13, 14, 15 & 16 | 53 | AC | 3,500 | 185,500 |
| <u>Contingency @ 15%</u> | | | | 1,082,331 |
| <u>Program Implementation @ 5%</u> | | | | 360,777 |
| <u>TOTAL ESTIMATED COST</u> | | | | \$ 10,287,256 |

CITY OF MERCED
Storm Drain Master Plan

Drainage Infrastructure Required to Serve Areas Draining Into Doane Lateral Canal
Cost Estimate

Table 7

Watershed H

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|----------|------|-----------|----------------------|
| <u>Detention Basins</u> | | | | |
| (Detention Basins 17, 18 & 19) | 335 | AF | 10,000 | 3,350,000 |
| <u>Channel</u> | | | | |
| 60' R/W | 2,500 | LF | 50 | 125,000 |
| <u>Pump Stations</u> | | | | |
| Detention Basin 17 | 1 | LS | 340,000 | 340,000 |
| Detention Basin 18 | 1 | LS | 453,000 | 453,000 |
| Detention Basin 19 | 1 | LS | 310,000 | 310,000 |
| <u>Storm Drain</u> | | | | |
| 30" SD | 1,248 | LF | 80 | 99,840 |
| 36" SD | 1,318 | LF | 100 | 131,800 |
| 42" SD | 6,073 | | 120 | 728,760 |
| 48" SD | 4,474 | LF | 130 | 581,620 |
| 54" SD | 8,746 | LF | 140 | 1,224,440 |
| 60" SD | 5,010 | LF | 160 | 801,600 |
| <u>Subtotal Construction</u> | | | | 8,146,060 |
| <u>Design & Planning @ 10%</u> | | | | 814,606 |
| <u>Construction Management @10%</u> | | | | 814,606 |
| <u>Land Acquisition</u> | | | | |
| Detention Basins 17, 18 & 19 | 69 | AC | 3,500 | 241,500 |
| Channel | 3 | AC | 3,500 | 11,900 |
| <u>Contingency @ 15%</u> | | | | 1,221,909 |
| <u>Program Implementation @ 5%</u> | | | | 407,303 |
| <u>TOTAL ESTIMATED COST</u> | | | | \$ 11,657,884 |

CITY OF MERCED
Storm Drain Master Plan

Drainage Infrastructure Required to Serve Areas Draining Into Farmdale Lateral
Cost Estimate

Table 7

Watershed I

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|-----------------|-------------|------------------|-------------------|
| <u>Detention Basin</u> | | | | |
| (Detention Basin 20) | 14 | AF | 10,000 | 140,000 |
| <u>Pump Station</u> | | | | |
| Detention Basin 20 | 1 | LS | 280,000 | 280,000 |
| <u>Storm Drain</u> | | | | |
| 36" SD | 1,310 | LF | 100 | 131,000 |
| 42" SD | 1,077 | LF | 120 | 129,240 |
| <u>Subtotal Construction</u> | | | | 680,240 |
| <u>Design & Planning @ 10%</u> | | | | 68,024 |
| <u>Construction Management @10%</u> | | | | 68,024 |
| <u>Land Acquisition</u> | | | | |
| Detention Basin 20 | 3 | AC | 3,500 | 10,500 |
| <u>Contingency @ 15%</u> | | | | 102,036 |
| <u>Program Implementation @ 5%</u> | | | | 34,012 |
| <u>TOTAL ESTIMATED COST</u> | | | | \$ 962,836 |

CITY OF MERCED
Storm Drain Master Plan
 Drainage Infrastructure Required to Serve Areas Draining Into Miles Creek
Cost Estimate

Table 7

Watershed J

| Item | Quantity | Unit | Unit Cost | Total Cost |
|---|-----------------|-------------|------------------|---------------------|
| <u>Detention Basin</u> (Detention Basin 21) | 33 | AF | 10,000 | 330,000 |
| <u>Pump Station</u> Detention Basin 21 | 1 | LS | 310,000 | 310,000 |
| <u>Storm Drain</u> 48" SD | 1,389 | LF | 130 | 180,570 |
| 54" SD | 940 | LF | 140 | 131,600 |
| <u>Subtotal Construction</u> | | | | 952,170 |
| <u>Design & Planning @ 10%</u> | | | | 95,217 |
| <u>Construction Management @10%</u> | | | | 95,217 |
| <u>Land Acquisition</u> Detention Basin 21 | 7 | AC | 3,500 | 24,500 |
| <u>Contingency @ 15%</u> | | | | 142,826 |
| <u>Program Implementation @ 5%</u> | | | | 47,609 |
| <u>TOTAL ESTIMATED COST</u> | | | | \$ 1,357,538 |

CITY OF MERCED
Storm Drain Master Plan

Drainage Infrastructure Required to Serve Areas Draining Into El Capitan Canal
Cost Estimate

Table 7

Watershed K

| Item | Quantity | Unit | Unit Cost | Total Cost |
|--|-----------------|-------------|------------------|---------------------|
| <u>Detention Basin</u> | | | | |
| (Detention Basin 22) | 24 | AF | 10,000 | 240,000 |
| <u>Pump Station</u> | | | | |
| Detention Basin 22 | 1 | LS | 280,000 | 280,000 |
| <u>Storm Drain</u> | | | | |
| 36" SD | 1,300 | LF | 100 | 130,000 |
| 42" SD | 1,200 | LF | 120 | 144,000 |
| <u>Subtotal Construction</u> | | | | 794,000 |
| <u>Design & Planning @ 10%</u> | | | | 79,400 |
| <u>Construction Management @10%</u> | | | | 79,400 |
| <u>Land Acquisition</u> | | | | |
| Detention Basin 22 | 5 | AC | 3,500 | 17,500 |
| <u>Contingency @ 15%</u> | | | | 119,100 |
| <u>Program Implementation @ 5%</u> | | | | 39,700 |
| <u>TOTAL ESTIMATED COST</u> | | | | \$ 1,129,100 |

EXHIBIT 'A'

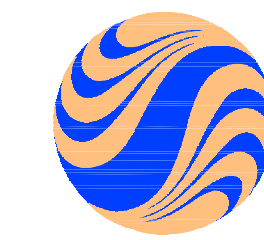
CITY OF MERCED STORM DRAIN MASTER PLAN

EXISTING CONDITIONS
Map Showing Watershed and Sub-Basin Boundaries,
Existing Storm Drain Trunk Lines,
Detention Ponds and Pump Stations and
10-yr Discharges.

CITY OF MERCED JOB NO. 199036

FINAL

PREPARED BY:

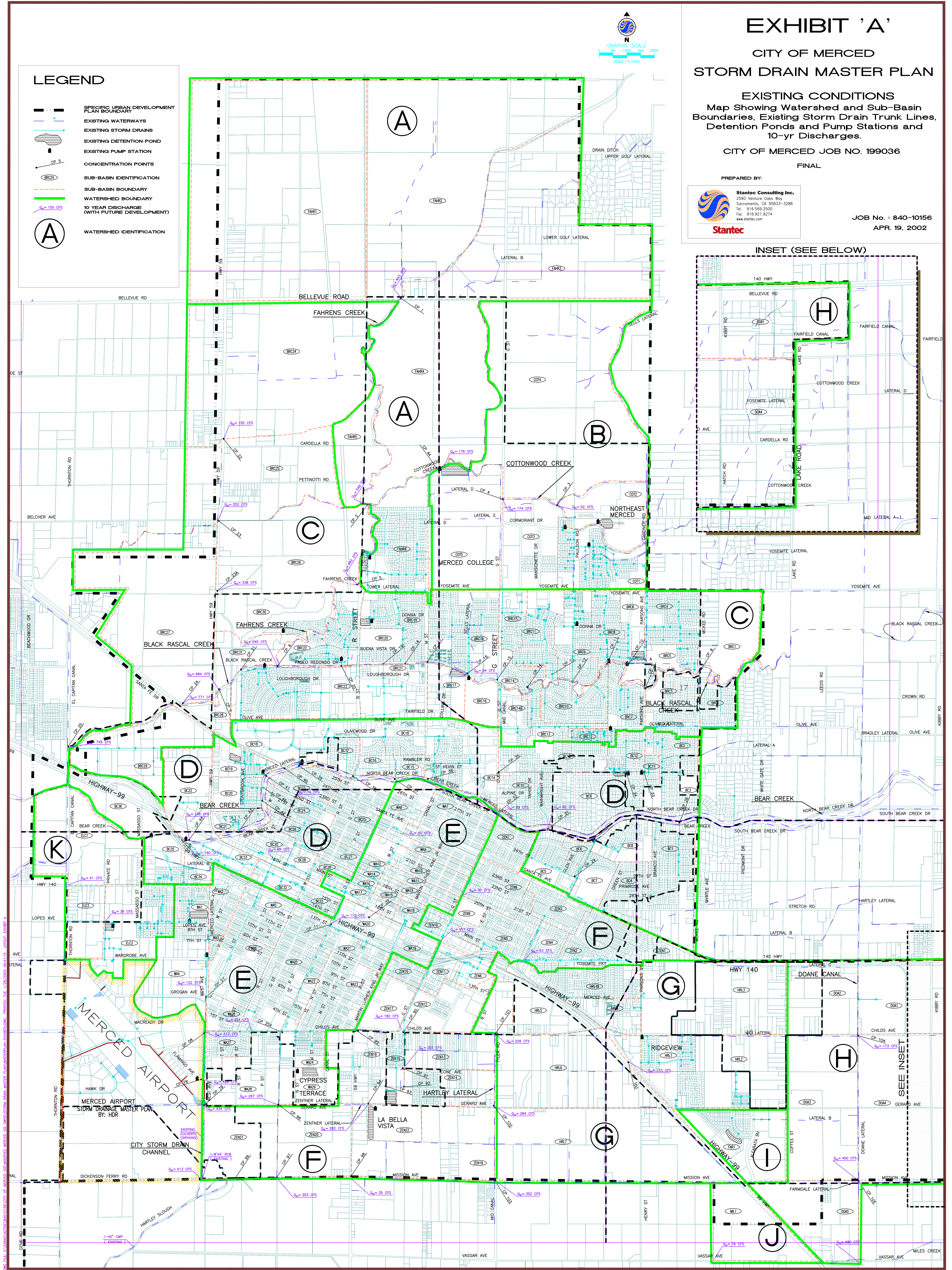
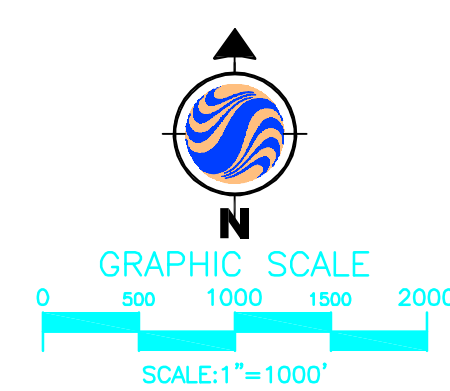


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Fax: 916.921.9274
www.stantec.com

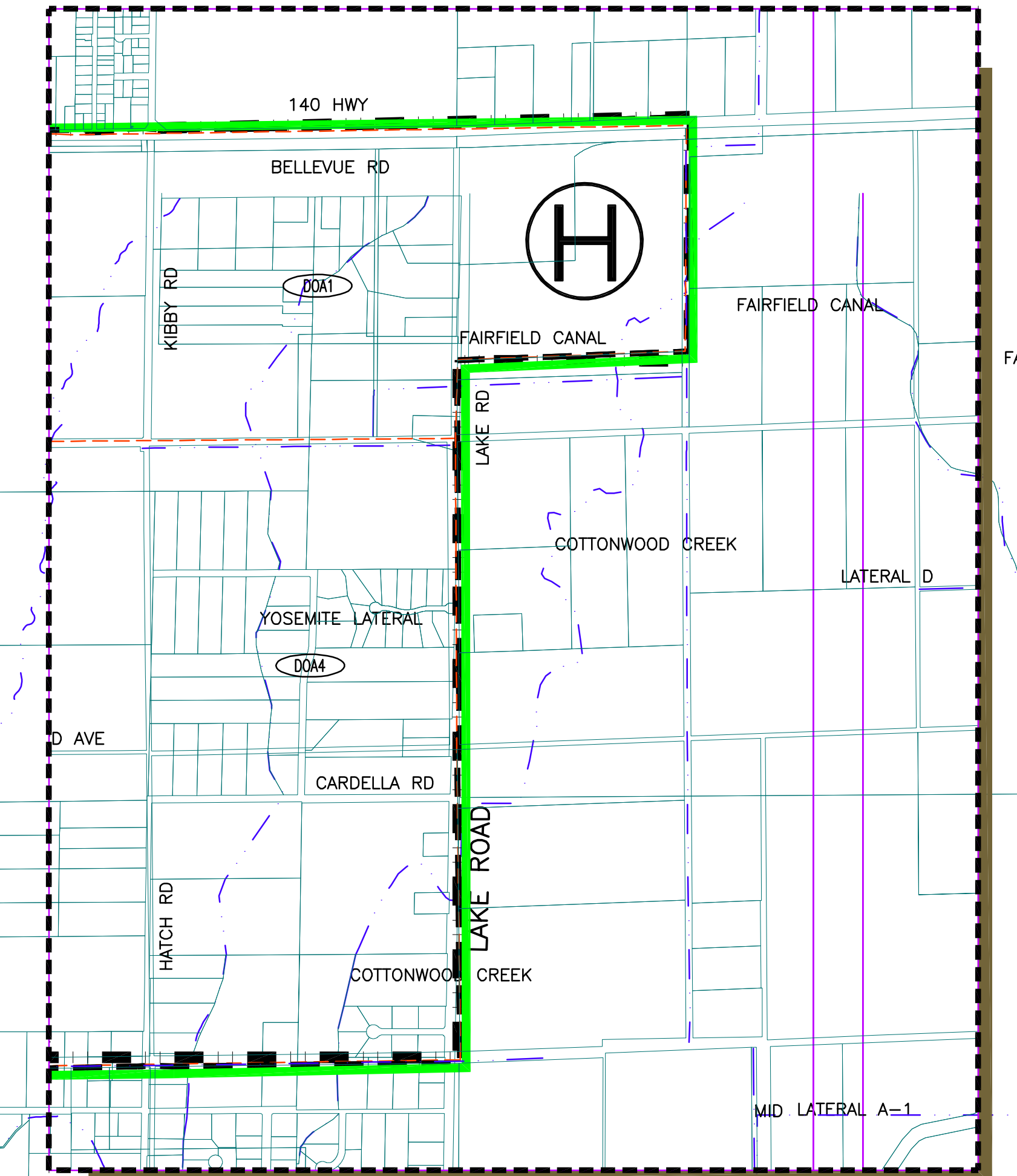
JOB No. : 840-10156
APR. 19, 2002

LEGEND

- SPECIFIC URBAN DEVELOPMENT PLAN BOUNDARY
- EXISTING WATERWAYS
- EXISTING STORM DRAINS
- EXISTING DETENTION POND
- EXISTING PUMP STATION
- CONCENTRATION POINTS
- SUB-BASIN IDENTIFICATION
- SUB-BASIN BOUNDARY
- WATERSHED BOUNDARY
- 10 YEAR DISCHARGE (WITH FUTURE DEVELOPMENT)
- WATERSHED IDENTIFICATION



INSET (SEE BELOW)



SEE INSET

FILE: C:\ADMINISTRATIVE\GIS\PROJECTS\STORM DRAIN MASTER PLAN\ADMINISTRATIVE\PRINTED\JOB 199036.DWG DATE: 4/19/02 10:41:15 AM

EXHIBIT 'B'

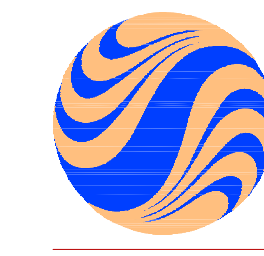
CITY OF MERCED STORM DRAIN MASTER PLAN

PROPOSED INFRASTRUCTURE Map Showing Proposed Storm Drain Trunk Lines, Detention Basins and Pump Stations CITY OF MERCED JOB NO. 199036

NOTE: PROPOSED STORM DRAINS SIZED FOR 10-YEAR EVENT, DETENTION BASINS SIZED FOR 50-YEAR (FUTURE) INFLOW / 2-YEAR (EXISTING) OUTFLOW PER CITY STANDARDS.

FINAL

PREPARED BY:



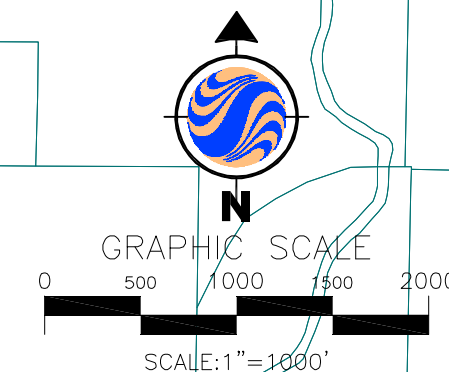
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APR. 19, 2002

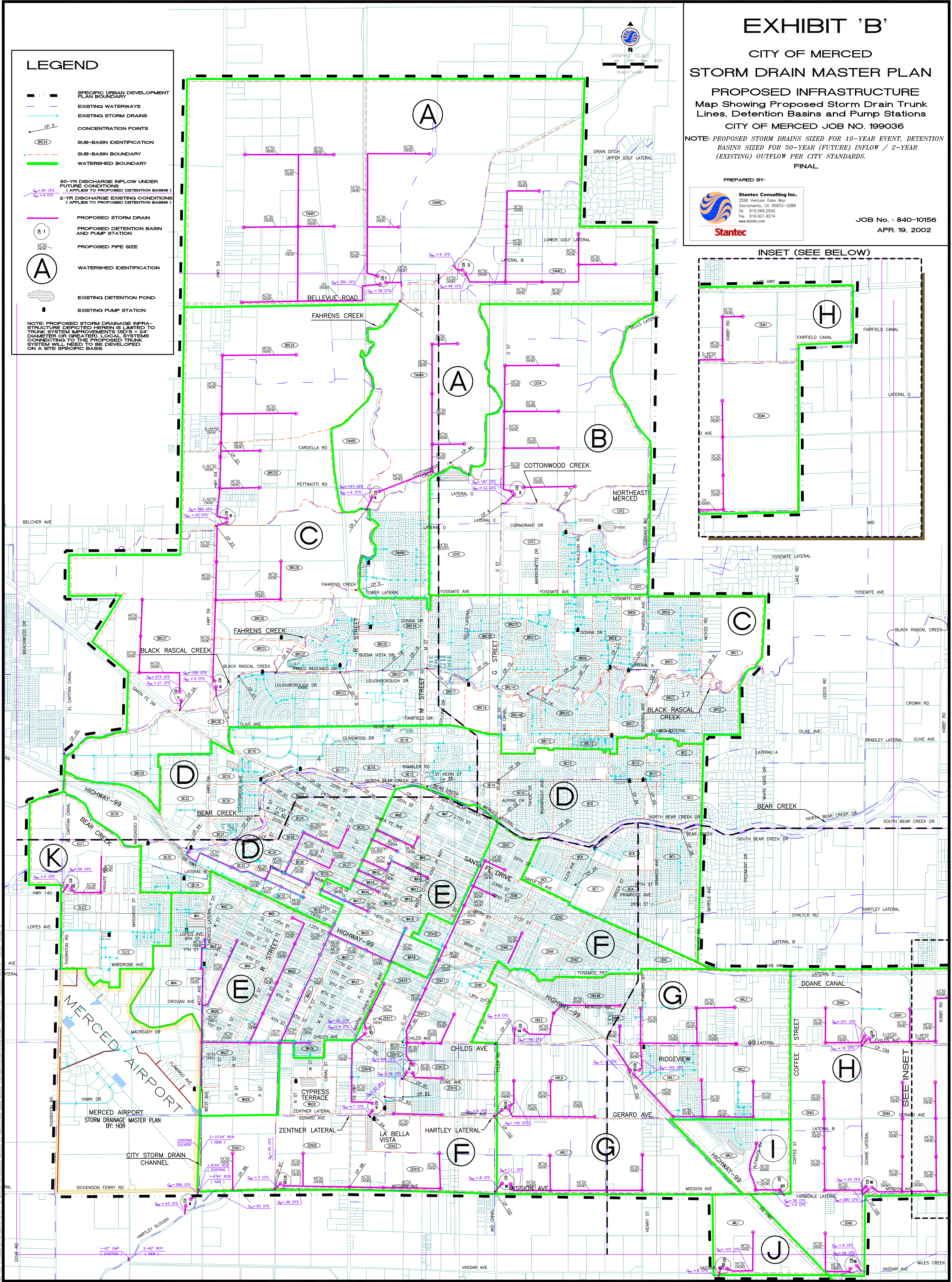
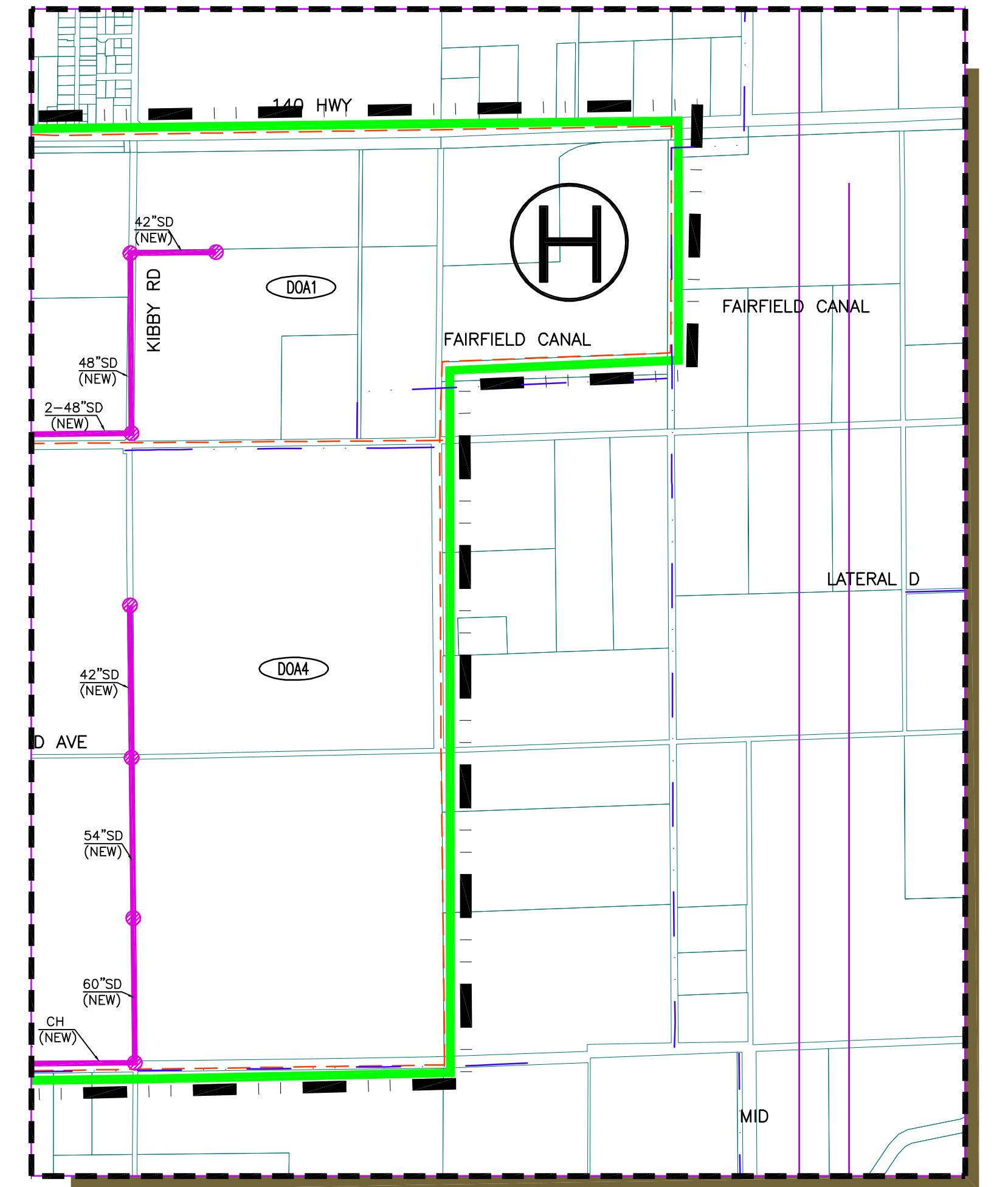
LEGEND

- SPECIFIC URBAN DEVELOPMENT PLAN BOUNDARY
- EXISTING WATERWAYS
- EXISTING STORM DRAINS
- CONCENTRATION POINTS
- SUB-BASIN IDENTIFICATION
- SUB-BASIN BOUNDARY
- WATERSHED BOUNDARY
- PROPOSED STORM DRAIN
- PROPOSED DETENTION BASIN AND PUMP STATION
- PROPOSED PIPE SIZE
- WATERSHED IDENTIFICATION
- EXISTING DETENTION POND
- EXISTING PUMP STATION

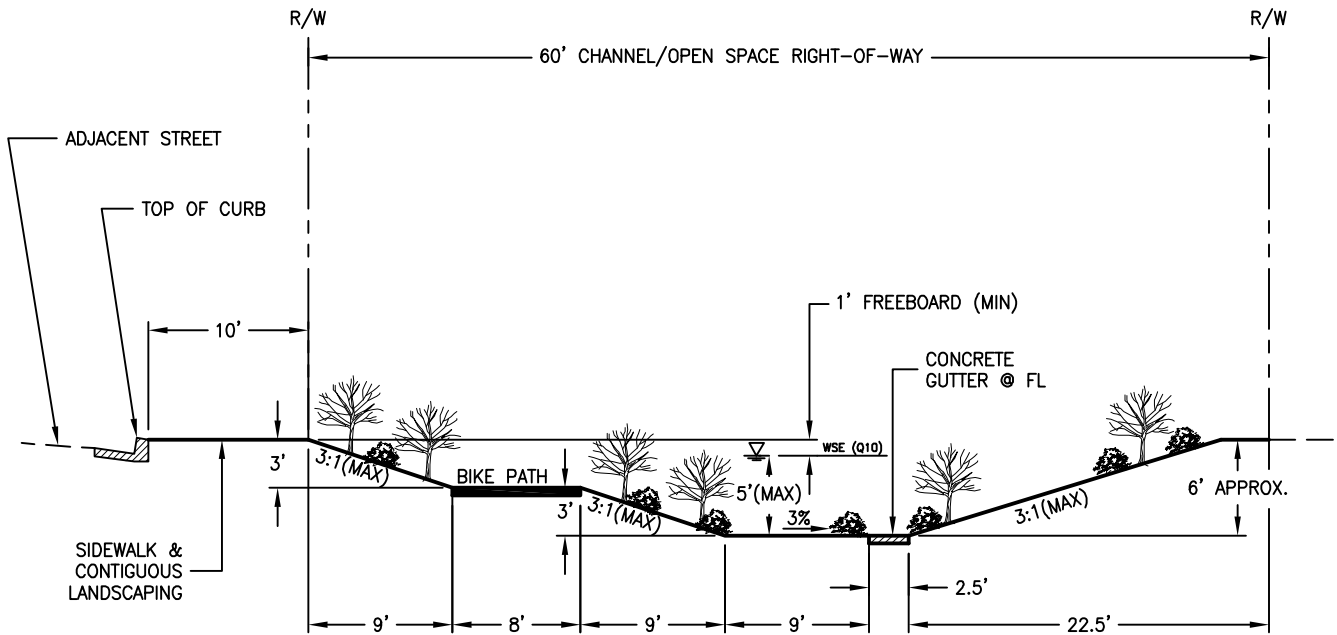
NOTE: PROPOSED STORM DRAINAGE INFRASTRUCTURE DEPICTED HEREIN IS LIMITED TO TRUNK SYSTEM IMPROVEMENTS (SD'S - 24" DIAMETER OR GREATER). LOCAL SYSTEMS CONNECTING TO THE PROPOSED TRUNK SYSTEM WILL NEED TO BE DEVELOPED ON A SITE SPECIFIC BASIS.



INSET (SEE BELOW)



CITY OF MERCED STORM DRAIN MASTER PLAN



60' RIGHT-OF-WAY CHANNEL CROSS-SECTION WITH BIKE PATH 3' ABOVE CHANNEL INVERT

NOTES:

1. ACCESS ROAD NOT NEEDED FOR CHANNEL REACHES THAT ARE LOCATED ADJACENT TO PUBLIC STREETS.
2. BIKE PATH ELEVATION TO UNDULATE BETWEEN 3' ABOVE CHANNEL BOTTOM AND TOP OF BANK.

**CITY OF MERCED
STORM DRAIN MASTER PLAN
EXHIBIT C**

| | |
|------------------------|------------------|
| DATE: 2/11/2002 | DRAWN: RAE |
| SCALE: NOT TO SCALE | SHEET: 1 OF 1 |
| JOB NO: 84010156 | |



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